

NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

A THREE-DIMENSIONAL TRANSONIC, POTENTIAL FLOW
COMPUTER PROGRAM, ITS CONVERSION TO IBM
FORTRAN AND UTILIZATION

by

Jack Paschall III

December 1983

Thesis Advisor:

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extensive; therefore, an interactive program was developed to aid the user in building the required input data file.

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A Three-Dimensional Transonic, Potential Flow Computer
Program, Its Conversion to IBM Fortran and Utilization

by

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Commander, United States Navy
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Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN AERONAUTICAL ENGINEERING

from the

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ABSTRACT

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I. INTRODUCTION

In the Aeronautical Engineering curriculum graduate level aerodynamics course, AE-4501, the students are exposed to two computer programs. One of these, prepared by the Douglas Aircraft Company, analyzes the potential flow around three-dimensional wings but is limited to incompressible flow [Ref. 1]. The other program, prepared by Cebeci, calculates the friction drag for two dimensional incompressible flow over airfoils [Ref. 2]. A serious defect of these programs is that they are not state-of-the-art computer programs. The Douglas program does not consider the effects of compressibility and the boundary layer program, in addition to being restricted to incompressible flow, does not predict the laminar to turbulent transition point.

A. BACKGROUND

In 1980 the Department of Aeronautics at the Naval Postgraduate School acquired an intricate computer program recently developed by the Boeing Commercial Airplane Company. This state-of-the-art program calculates three-dimensional transonic flow over wings and bodies in

both the outer-inviscid flow region governed by the transonic potential equation and the thin layer in which the first order, compressible boundary layer equations are assumed to be valid.

The Boeing program as received was designed to be executed on a CDC 6600 or a CYBER 175 computer and was written using CDC FORTRAN IV extended language. This thesis therefore was primarily concerned with the conversion of the program to FORTRAN IV extended compatible with the Naval Postgraduate School's (NPS) IBM 3033 system. The large modular program was divided so that the potential flow analysis portion could be run separately. Simplified instructions for use of the program were also prepared.

B. VISCOUS/INVISCID SYSTEM OF PROGRAMS

The Viscous/Inviscid Wing System (VIWS) of programs calculates three-dimensional transonic flow over wings and wing body combinations including details of the laminar or turbulent flow in the three-dimensional viscous boundary layer. The flow field is calculated in two overlapping regions: an outer inviscid flow region governed by the transonic potential equation, and a thin boundary layer in which the first order, three-dimensional, compressible

boundary layer equations are assumed to hold and in which the effects of surface heat and mass transfer can be computed. A list of the VIWS of programs is presented in Table I.

TABLE I
Viscous/Inviscid Wing System of Programs

Program Name	Description
F1027	Jameson-Caughey inviscid, transonic wing code
A411IN	Reads geometry & velocity data, constructs coordinate system
VWIN	Potential flow boundary layer interface
A411AC1	Three-dimensional boundary layer program
INTERP	Boundary layer potential flow interface
A411F1 A411P2 A411FS	Graphics display programs

The basic sequence of calculations used by the VIWS to obtain matched viscous and inviscid solutions consists of an iterative loop in which the inviscid outer flow analysis and the boundary layer analysis are performed sequentially. The iterative sequence is continued until either convergence (satisfactory matching) is achieved, or the maximum number of iterations specified by the user has been performed. The VIWS programming sequence is shown schematically in Fig. 1.1.

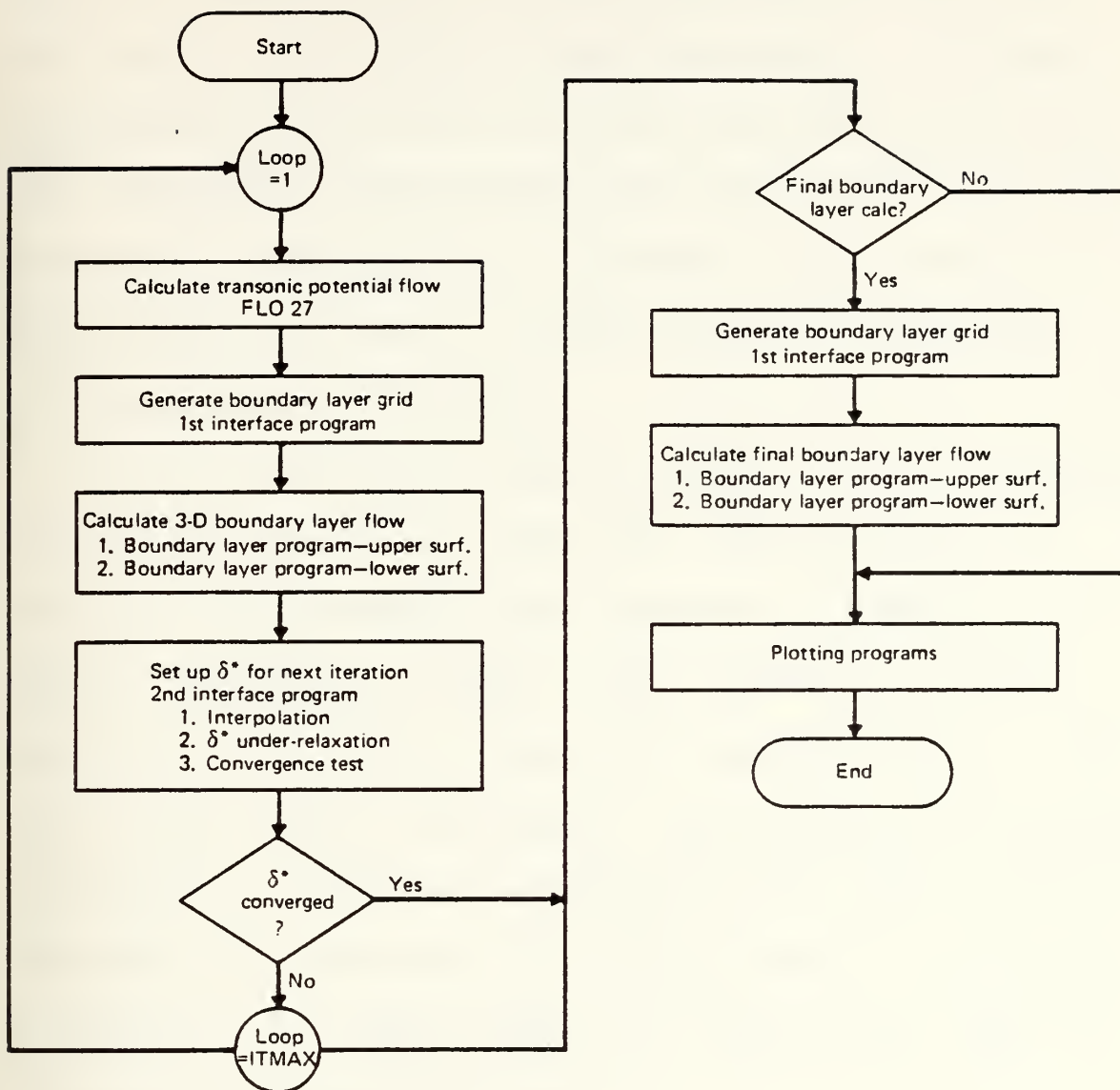


Figure 1.1. Viscous/Inviscid Interaction Procedure

The potential flow is calculated for the bare wing during the first iteration. In subsequent iterations, the effect of the boundary layer flow on the outer inviscid flow is

felt as a modification to the wing shape through the addition of the boundary layer displacement thickness. Convergence is recognized, and the iterations are stopped, when the maximum change between the new and old displacement thickness, expressed as a fraction of the maximum displacement thickness, is less than the convergence tolerance chosen by the user.

The VIWS utilizes the Jameson-Caughey transonic inviscid wing program FLO27, to carry out the potential flow analysis. The boundary layer analysis is performed by a finite difference boundary layer prediction program developed by the Boeing Commercial Airplane Company. The basic theory behind the boundary layer program is contained in [Ref. 3]. A detailed description of the VIWS of programs (excluding the potential flow program FLO27) is contained in [Ref. 4]. A basic guide to the use of the VIWS of programs is contained in [Ref. 5].

II. POTENTIAL FLOW PROGRAM FLO27

Because of the extensive length and number of program modules in the VIWS, the Potential Flow Program, FLO27, was singled out for conversion. It was anticipated that FLO27 would be run separately at first and recombined with the other program modules at some later date when these modules were themselves translated for execution on the IBM 3033 computer.

A. RE-PROGRAMING

The Potential Flow Program, hereafter called FLO27, was received on magnetic tape and loaded into the IBM 3033 mass storage system using the Job Control Language (JCL) routines presented in Appendix A. The magnetic tape contained twenty (20) total files in which the format was 9 track, 1600 CPI, unlabeled. The card image format for the sixteen (16) program files is 80 characters per record and the four (4) output files contain 150 characters per record. The program and output files on the original CDC tape are listed in Table II.

The FLO27 program was converted to FORTRAN IV extended suitable for execution on the IBM computer using the NPS CDC

TABLE II
CDC Magnetic Tape Files

File/Records	Name	Description
1 /2356	FL027	Potential Flow Program
2 /3194	A411IN	Reads geometry & velocity data constructs coordinate system
3 / 378	VWIN	Potential flow boundary-layer interface
4 /6611	A411AO1	Three-dimensional boundary layer program
5 /1977	INTERP	Boundary-layer potential flow interface
6 / 688	A411PS	Streamline plots
7 / 211	A411P1	One-dimensional plots
8 / 586	A411P2	Contour plots
9 / 70	COUPLE	Procedure files
10 / 158	ITER	
11 / 7	DATAIN	
12 / 78	FINAL	
13 / 434	BOEB1	Boeing McLean computer program
14 / 36	CONTPLT	Contour plots
15 / 17	CORDPLT	One-dimensional plots
16 / 40	STREPLT	Streamwise plots
17	OUTF27	Output from FL027
18	OUTIFC	Output from VWIN
19	OUT411L	Output from boundary-layer, lower surface
20	OUT411U	Output from boundary-layer, upper surface

to IFM conversion guide [Ref. 6]. The first step taken consisted of program compilation using the WATFIV compiler with its extended error messages. The listing which was

produced flagged all areas of the program which required revision. Program changes were accomplished utilizing this WATFIV listing. Some of the more general and repetitive changes are listed in Table III.

TABLE III

FLO27 Re-Programming Changes

CDC Code	IBM Code Change
Variables: FREAD, FREAF, FWRIT, FWRIF, IREAD, IREAF, IWRIT, IWRIF	Eliminated from program
WRITE(IWRIT,600)	WRITE(6,600)
READ(IREAF,500)	READ(5,500)
READ 7, WRITE 7 or REWIND 7	Changed to READ 14, WRITE 14 or REWIND 14
Call SECCND(T)	Step eliminated
Call SSWITCH(1,ISTOP)	Call SLITET(1,ISTOP)
Delimiter of form *	Replaced by '
Comment cards with *	Replaced by C
LEVEL statement	Step eliminated
If(UNIT(N).GT.0.) GO TC	All of this type eliminated

The most difficult change to make occurred with the CDC Buffer IN or Buffer OUT statements which were used in the program to transfer portions of a three-dimensional array into and out of main memory. The Buffer routines reduce the memory size required to execute the program. This statement type occurred in the main program and several of the subroutines.

The change required to translate this statement is presented below with the CDC code preceeding the IBM FORTRAN.

EOUFFER OUT (N3,1) (G(1,1,1),G(MX,MY,1)) changed to

WRITE(N3) ((G(I,J,1),I=1,MX),J=1,MY) and

EOUFFER IN (N1,1) (G(1,1,M),G(MX,MY,M)) changed to

READ(N1,ERR=) ((G(I,J,M),I=1,MX),J=1,MY)

The variable ERR was assigned the GO TO statement number of the UNIT statement immediately following the BUFFER IN line of code. As an example, if the UNIT statement following the EUFFER IN code was - If(UNIT(N1).GT.0.) GO TO 151, then the number 151 was assigned to variable ERR following the equal sign. All CDC UNIT statements were eliminated from the FLO27 source code per Table II.

In addition to the program changes required to run FLO27 on the IBM computer, several lines of code were added to modify the output format to a more usable form. A subroutine, VERTEC, which calls the Versatec plotter was also added to enhance program usefulness. This plotting routine is user controlled through an input variable and is explained in the next section. The modified FLO27 program source code is presented in Appendix E.

To facilitate program data entry several input variables which had recommended values were initialized to these values within the Main program and the subroutine GEOM. The initialized input variables and their values are presented in Table IV.

TABLE IV
Initialized Input Variables

AREA	VARIABLE NAME	INITIALIZED VALUE
MAIN Prgm.	XSCAL	0.0
	PSCAL	0.0
	FCONT	0.0
	P20	0.7
	P30	1.0
	FSMCO	0.0
	PTMAP	0.0
	BLCP	0.0
	WEIG	1.0
	PTCK	0.0
	FIX	0.0
Subrt. GEOM	YSYM	0.0
	FNB	2.0
	PX	0.0
	PZ	0.0
	TRL	0.0
	SLT	0.0
	XSING	0.0
	YSING	0.0

A complete description of each input variable in Table IV can be found on pages 19 through 23 of [Ref. 5].

B. PROGRAM DESCRIPTION

The FLC27 program is a computer code written to analyze the transonic flow over a wing alone or a wing on a cylindrical fuselage. It uses a finite-volume formulation to solve the exact potential flow equation in conservative form. In the development of the equations, the basic assumptions are; steady flow, no heat or work transfer, isentropic flow, irrotational flow, no body forces and a perfect gas. The velocity vector in cartesian coordinates is

$$\vec{V} = u\hat{i} + v\hat{j} + w\hat{k} \quad (2.1)$$

where u , v and w are the velocity components. The continuity equation, assuming steady flow, is

$$\frac{\partial}{\partial x}(\rho u) + \frac{\partial}{\partial y}(\rho v) + \frac{\partial}{\partial z}(\rho w) = 0 \quad (2.2)$$

Next a velocity potential is introduced such that the velocity components are calculated as the gradient of this potential.

$$u = \phi_x, \quad v = \phi_y, \quad w = \phi_z \quad (2.3)$$

With the introduction of the velocity potential, the continuity equation 2.2 becomes

$$\frac{\partial}{\partial x}(\rho \phi_x) + \frac{\partial}{\partial y}(\rho \phi_y) + \frac{\partial}{\partial z}(\rho \phi_z) = 0 \quad (2.4)$$

Assuming no heat or work transfer, the energy equation can be written as

$$T \left[1 + \frac{(\gamma - 1)}{2} M^2 \right] = T_\infty \left[1 + \frac{(\gamma - 1)}{2} M_\infty^2 \right] \quad (2.5)$$

The flow is assumed to be uniform in the far field. On the surface of the body, the normal velocity component is zero. The velocities and densities of the near field are normalized using the free stream velocity and density, thus $V_\infty = 1$ and $\rho_\infty = 1$. Using the assumptions that the flow is isentropic and a perfect gas, the energy equation 2.5 can be shown to be

$$\rho = \left[1 + \frac{(\gamma - 1)}{2} M_\infty^2 (1 - v^2) \right]^{-\frac{1}{\gamma - 1}} \quad (2.6)$$

With equations 2.5 and 2.6 there are only two unknowns, ϕ and ρ . They can be solved, subject to the boundary condition of flow tangency, using a finite volume technique. The basic numerical scheme for the solution is the

construction of a mesh from small volume elements (cubes) which are packed around the wing or wing body configuration. The cubes in the computational domain are separately mapped to distorted cubes in the physical domain by independent transformations from local coordinates X , Y and Z to Cartesian coordinates x , y and z . The mesh points are the vertices (corners) of the mapped cubes. The velocity potential and density are calculated at each vertex in the mesh. The pressure distribution can then be calculated from

$$P = \frac{\rho^\sigma}{\gamma M_\infty^2} \quad (2.7)$$

In the event that the local flow velocity becomes supersonic and shocks occur, these are handled in the usual manner by insuring that:

- 1) The tangential velocity components are equal on each side of the shock.
- 2) Continuity is maintained by keeping the product of ρU_n constant across the shock (where U_n is the normal velocity component).
- 3) Discontinuous expansions (corresponding to an "expansion shock") are excluded from the flow field.

The assumption of isentropic flow along with the existence of shocks presents a contradiction which can only be resolved by limiting the flow to very weak shocks for which entropy and vorticity generation may be ignored. Thus, solutions will be valid only for subsonic free stream velocities.

The main three-dimensional array containing the potential function data is stored on disk, and special unformatted input/output statements are used to bring planes of data into central computer memory and to store updated planes of data back on the disk. In the construction of the computational coordinate system, a Joukowski transformation is used to transform the cylindrical fuselage to a vertical slit and then a sheared parabolic transformation is used in planes containing the airfoil sections. A detailed mathematical formulation of the potential flow analysis is contained in [Ref. 7].

1. Program Input

The input to FLO27 consists of variables which are read with an 8F10.6 FORMAT. Each input card has a title card which precedes it. This title card contains the input variable name and effectively labels the input data for easy

reference. The title for each input data is placed in the same column as the input data it labels. The title cards are read with a 20A4 FORMAT. All numerical input values are real numbers. The following data deck, listed card by card, is the minimum input data required for a simple wing analysis. Each "card" can be interpreted as one line of data on your terminal. A complete sample data set is presented in Appendix C.

CARD 1 The Run Title (64 characters maximum)

CARD 2 Title card for the input variables
FNX, FNY, FNZ, FMESH and FPIOT

CARD 3

Cols. 1-10 FNX - Number of computational cells in the chordwise direction for the initial mesh.

$MAX = 160/2^{**}n$, where $n = FMESH - 1$. (See Cols. 31-40 for FMESH)

Cols. 11-20 FNY - Number of computational cells in the normal direction from the airfoil surface for the initial mesh.

$MAX = 16/2^{**}n$, where $n = FMESH - 1$.

Cols. 21-30 FNZ - Number of computational cells in the spanwise direction for the initial mesh.

$MAX = 32/2^{**}n$, where $n = FMESH - 1$.

Cols. 31-40 FMESH - Determines the number of times a program generated computational mesh is refined. Enter only 1.0, 2.0 or 3.0 for coarse, medium or fine mesh. If 3.0 is selected the program will calculate flow over the wing for the coarse mesh then half the mesh size (medium), recalculate, then half the mesh again (fine) and do a final potential flow calculation. Output parameters are printed for each mesh size for which calculations were performed.

Cols. 41-50 FELOT - Output flag

0.0 = Normal output without printer-plot of C_p

1.0 = Normal output with printer-plot of C_p
at each computational mesh point for
each wing section.

2.0 = Normal output with Versatec plots of
 C_p versus X/C for each wing section of
the final mesh.

CARD 4 Title card for the input variables

FIT, COVO and P10

CARD 5-M One card for each computational mesh. Total
number of cards equal to $M = FMESH$.

Cols. 1-10 FIT - A parameter which fixes the maximum number of iterations the program will use to converge the velocity potential to a specified tolerance (COVO). This parameter must be repeated for each mesh refinement.

Cols. 11-20 COVO - Velocity potential convergence criteria. This input variable is also entered for each selected mesh. A value of 0.000001 is recommended.

Cols. 21-30 P10 - This parameter determines the subsonic point relaxation factor for the specified mesh size. A value of less than 2.0 must be entered for each designated mesh. Recommended values are: 1.6 for coarse, 1.3 for medium and 1.2 for the fine mesh.

CARD 6 Title card for the input variables
FMACH, YA, AL and CDO

CARD 7

Cols. 1-10 FMACH - Free stream Mach number

Cols. 11-20 YA - Yaw angle in degrees

Cols. 21-30 AL - Angle of attack in degrees

Cols. 31-40 CD0 - Drag coefficient due to skin friction. Unless known, an estimated value of 0.01 is recommended.

CARD 8 Title card for the input variables
ZSYM, FNS, SWEEP, DIHED and FUS

CARD 9

Cols. 1-10 ZSYM - The wing planform symmetry trigger.

0.0 = Yawed wing, has no spanwise symmetry

1.0 = Swept wing, has spanwise symmetry

Cols. 11-20 FNS - This input variable tells the program the total number of wing sections you have selected to define the wing half span. The number must be at least three (3) but not more than eleven (11) sections.

Cols. 21-30 SWEEP - Leading edge sweep angle in degrees.

Cols. 31-40 DIHED - Dihedral angle in degrees. See
Fig. 2.1.

Cols. 41-50 FUS - Input the fuselage radius. Enter 0.0 for a wing-alone case.

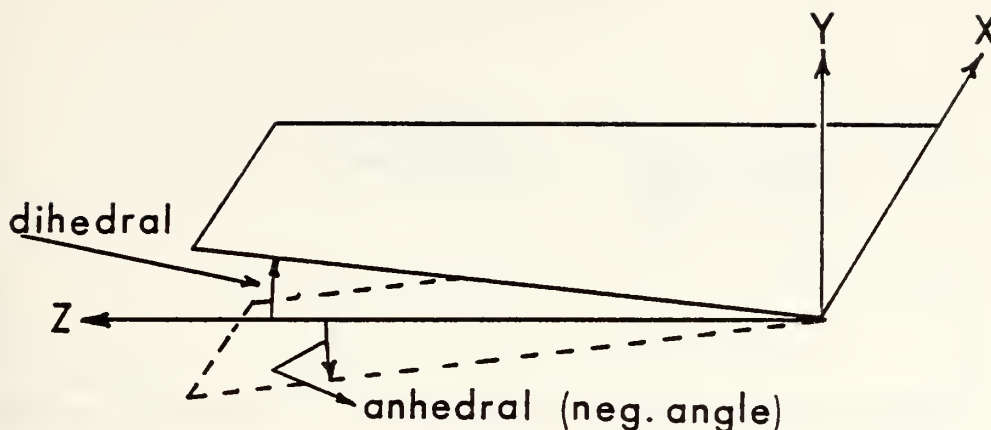


Figure 2.1. Dihedral Angle

Data input cards from 10 through 15 are used for defining wing planforms and section geometrics. For the first wing section, all data cards from card 10 through card 15 must be used. For the second and subsequent sections there is an option for skipping the wing section defining data (cards 12 through 15) and copying the data from that of the previous section. This option is controlled by the input variable FSEC. If this option is not used, data cards from 10 through 15 must be repeated for each wing defining section. The number of wing sections which are defined is input with the variable FNS. Remember, up to 11 sections may be defined, and a minimum of 3 sections must be defined. All wing planform and section defining geometrics must be in consistent units. Wing planform and section defining quantities are presented in Fig. 2.2.

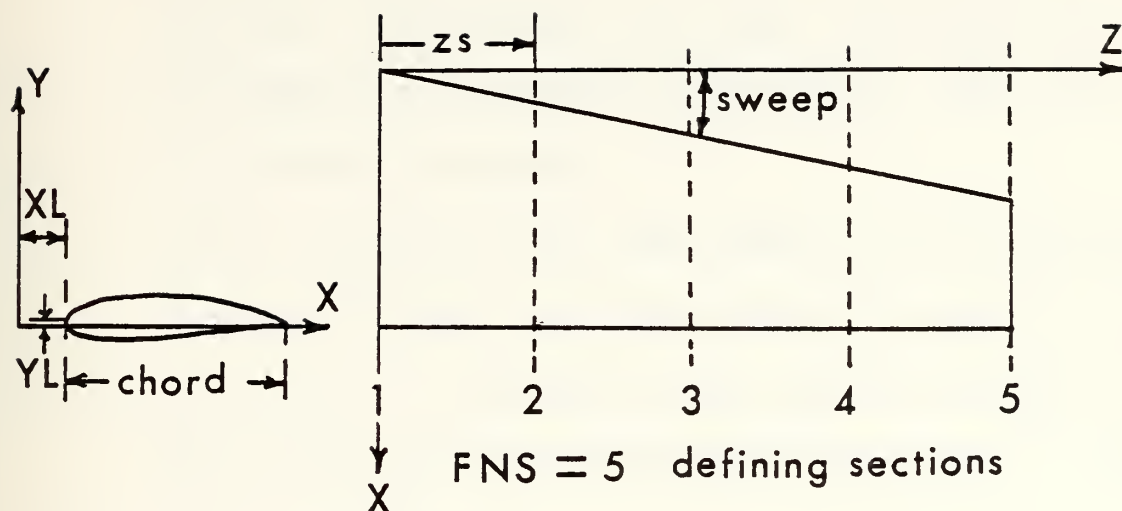


Figure 2.2. Wing Defining Geometry

CARD 10 Title card for the input variables

ZS, XI, YL, CHORD, THICK, AT and FSEC

CARD 11

Cols. 1-10 ZS - The section spanwise coordinate

(Start at the centerline and work
outboard)

Cols. 11-20 XL - Section leading edge X coordinate

Cols. 21-30 YL - Section leading edge Y coordinate

Cols. 31-40 CHORD - Section chord length

Cols. 41-50 THICK - The thickness scaling factor can be used to scale all Y coordinates of the wing section. Thus percent thickness and camber are increased (or decreased) accordingly. Use 1.0 if no scaling is desired.

Cols. 51-60 AT - The twist angle of each section (geometric twist) measured from the X axis to the chord line. A positive twist angle reduces the section angle of attack and gives "washout". Use 0.0 for no twist.

Cols. 61-70 FSEC - This is a flag which determines whether or not the program reads wing section defining geometry from a previous wing section or from new defining geometry. For the first section defined you must set FSEC to 1.0. Following the first section, if you define new section geometry then use FSEC = 1.0. If you want the program to read the section geometry defined from the previous section then set FSEC = 0.0.

CARD 12 Title card for the input variable

FN

CARD 13

Ccls. 1-10 FN - This variable contains the number of points which define the upper and lower surface of the section. A maximum of 161 points may be used.

CARD 14 Title card for the input variables

XF(I) and YP(I)

CARDS 15-1 to 15-N Total number of cards equals N,

where $N = \text{integer part of } (FN+2)/3$.

The X and Y coordinates at each point are entered in pairs, three points to a card. (See Appendix C for sample input)

Ccls. 1-10 XP(I) - X coordinate of the wing
section point

11-20 YP(I) - Y coordinate of the wing
section point

21-30 defining X coordinate for next
point

31-40 defining Y coordinate for next
point

41-50 defining X coordinate for
following point

defining Y coordinate for
following point

The X and Y coordinates of the wing section defining points must be entered starting with the upper surface trailing edge point and proceeding along the upper surface to the leading edge, and returning along the lower surface to the lower surface trailing edge point. It is very important to define the section leading edge with a large number of closely spaced points. Suggest at least 0.05 spacing or less between X coordinate values from 0.1 X/C to the leading edge, $X/C = 0.0$. Each X and Y coordinate point is normalized using the chord length for that section. Section defining geometrics are illustrated in Fig. 2.3.

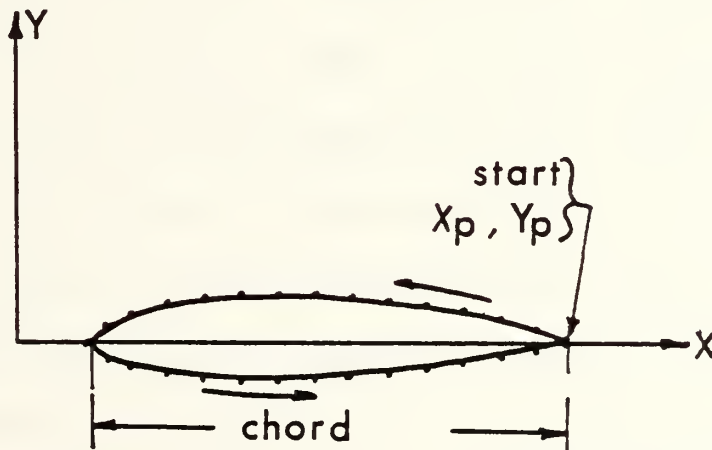


Figure 2.3. Section Defining Geometry

CARD 16 Title card containing the words in Cols. 1-80

END OF CALCULATIONS

CARD 17 Title card for the input variable

FNX

CARD 18

Cols. 1-10 FNX - This variable indicates the end of a set of calculations and must be set equal to 0.0. Its purpose is to indicate that the program has run to completion.

2. Program Output

Output from the FLO27 program varies with the value of the input variable FPLCT. When FPLCT is set equal to 0.0 a normal output is produced. This normal output contains (in order of occurrence): refined input geometry data including trailing edge slope and angle calculations; iterative solution of the potential flow mesh; section characteristics and wing characteristics. The iterative solution, section and wing characteristic data are repeated for each mesh refinement requested. Thus, if the input variable FMESH is set equal to 3, these data are calculated and output three times. The last data in the normal output consists of the non-dimensionalized chord (X/C) and pressure

coefficient (C_p) data at each computational mesh point for each wing section calculated during the final mesh. A sample of the normal output data is presented in Appendix D and represents the output data from Appendix C input data.

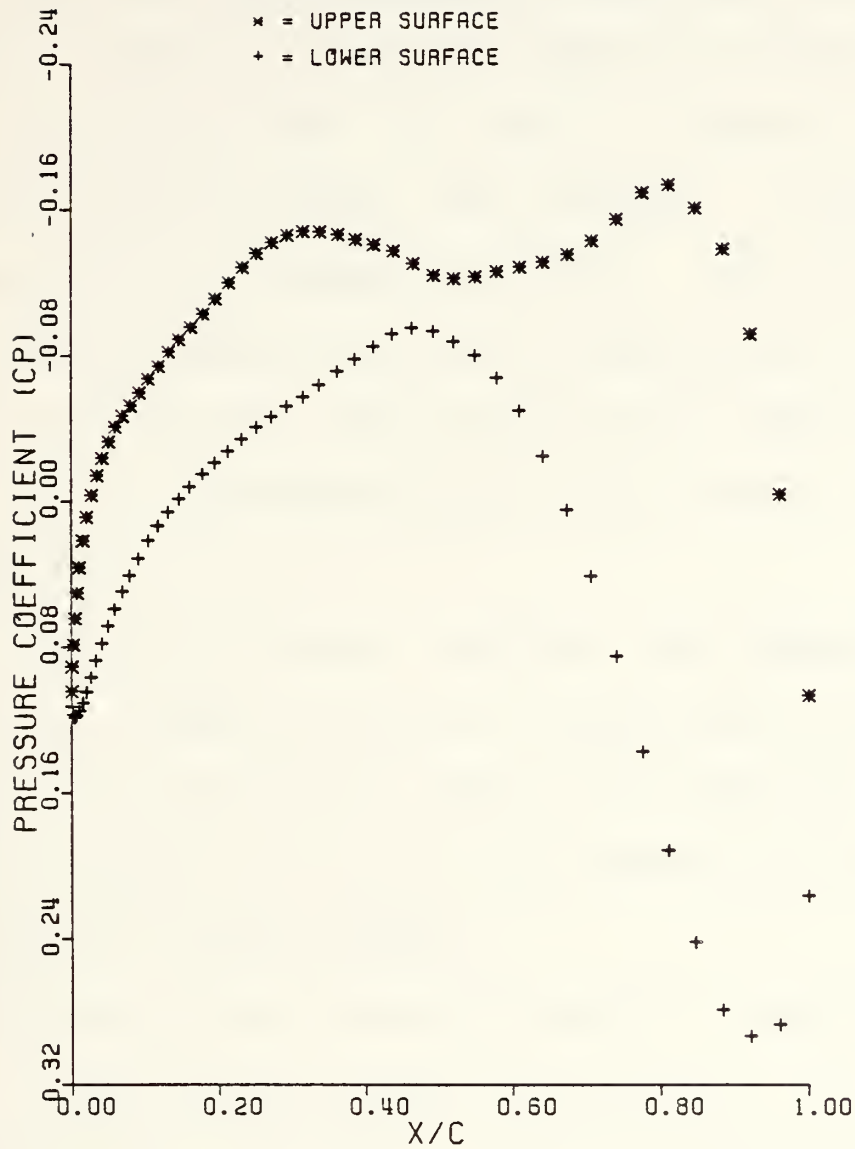
If variable FPLOTT is set equal to 1.0, the output data is increased considerably. This output contains the normal output plus a line printer-plot of the pressure coefficient at each computational mesh point for each wing section. The line printer-plot is produced for each wing section of each mesh refinement. The length of the output data with FPLOTT set equal to 1.0 can approach 6000 records depending on the number of mesh refinements requested. These plots are of questionable value and, therefore, an alternate plotting program was developed.

When the variable FPLOTT is set equal to 2.0, the normal output data is produced plus a Versatec plotting subroutine (VERTEC) is called. The subroutine outputs, via the Versatec plotter, plots of C_p versus X/C for each wing section of the final mesh calculations. This routine is simply putting into plot form the C_p and X/C numerical data contained in the normal output. A sample of the Versatec plot is presented in Fig. 2.4.

SECTION CP DATA

* = UPPER SURFACE

+ = LOWER SURFACE



SPAN STATION = 2.550

MACH 0.800

YAW 0.000

AOA 2.000

CL 0.34675

CD 0.02234

CM 0.00123

Figure 2.4. Versatec Plot of Cp vs. X/C

III. INTERACTIVE INPUT PROGRAM FLO27IN

The input data file required for the FLO27 program is extensive. Errors in input data FORMAT will cause program errors at execution time. In order to eliminate these errors and reduce the input data workload, a computer terminal interactive program was written. This interactive program, called FLO27IN, is a user-friendly way of creating an input data file for the potential flow wing analysis program FLO27. The FLO27IN program source code is presented in Appendix F.

The interactive program, FLO27IN, when executed ask's questions of the user in order to construct and write to the user's "A" disk the required FLO27 input data file. The following presents the step-by-step procedure for executing the interactive program FLO27IN.

STEP #1---Log on to any IBM 3033 interactive terminal
with your user number and password.

STEP #2---Once logged on and in the CMS operation mode
type:

CP LINK 0247P 191 120 RR then hit ENTER

STEP #3---The word PASSWORD will appear, Type and ENTER

AERO

STEP #4---Type and ENTER

ACC 120 D

STEP #5---Type and ENTER

LOAD FLO27IN (START

The screen will display the header for the interactive program. Answer each question presented. At the end of each question in parenthesis is the input data variable associated with that question and whether the input parameter is a real number (R) or an integer (I). Example:
==> Enter the free stream Mach number (FMACH): (R). FMACH is the input data variable for the question. As you proceed through the FLO27IN program, opportunities to review and change input data will be presented. Should it become necessary to change your input data after completing the FLO27IN program, you can simply XEDIT the created data file.

The FLO27IN program also incorporates a library which contains the wing-section defining data for a number of current wing shapes. A copy of this library is presented in Appendix B. This feature will be displayed during program execution by the use of a menu from which the user can select a pre-defined wing section or define his own.

Upon completion of user inputs to the interactive program three additional data lines are automatically written to the bottom of the input file. They are:

END OF CALCULATION

FNX

0.0

In addition, Job Control Language (JCL) cards are written to the top and bottom of the file. All JCL cards start with a // format. After FLO27IN has run to completion type and enter RELEASE 191 to release the aere disk which was linked while executing the FLO27IN program. The created data file is written to the user's "A" disk with <filename> <filetype> of FLO27 DATAIN. Additional changes can be made simply by entering the XEDIT mode and editing the file.

IV. FLO27 BAICH SYSTEM EXECUTION

The potential flow program FLO27 can be executed after the input data file has been created. The batch processor is required for FLO27 execution because of the extensive CPU time needed to run the program. While in the XEDIT mode, a standard JOB card must be added to the top of the FLO27 DATAIN file prior to submission for job execution. The JOB card has the form:

```
//jobname JOB (nnnn,pppp),'ident',CLASS=J
```

jobname = may contain up to 8 alphanumeric characters,

the first of which must be alphabetic.

nnnn = your user number

pppp = project number, assigned by professor

'ident' = contains the user's own identification

information. A maximum of 20 characters may be contained within the single quotation marks.

After adding the JOB card to your data file, you are ready to execute the program. Type SUBMIT FLO27 DATAIN and press ENTER. Batch runs are normally not worth waiting for. To inquire about the status of the job, enter INQ and the job name used on the JOB card or "logoff". If the system is busy and the maximum mesh size was selected, it may be several hours before your job is run.

When the job is run the output will be spooled to the batch printer located next to the VM printer in the main computer building. The title at the top of the printout for batch jobs is the name entered on the JOB card. If it is desired to have the program output data spooled directly to the terminal, it will be necessary to add one additional JCL card to the input data set. This card must be placed immediately following the JOB card and has the form:

```
//*MAIN ORG=NPGVM1.nnnnP
```

where nnnn = your user number

Inserting this card in the input data will cause all program output to be spooled to the user's virtual reader where it may be looked at, printed or transferred to his "A" disk. To enquire as to whether information is in the reader simply type RDR and hit enter, then follow the instructions on the screen.

V. PROGFAM TEST RESULTS

The FLO27 program was tested in three stages; (1) during the reprogramming phase for conversion completeness, (2) after successful conversion with suitable wing data for program accuracy and (3) during an AE-4501 class project.

A. ACCEPTANCE TEST DATA

To test and ensure that the FLO27 program was converted to IBM compatible Fortran without error, an acceptance test data set was used. The acceptance test input and output data was supplied with the original CDC program source code. After conversion of the FLO27 program to Fortran suitable for the NPS IBM system, the acceptance test input data were run and the output results compared to the output generated by the CDC system.

Both output data sets were numerically exact when the FLO27 program was run in double precision on the IBM system. If the program was run in single precision, the numerical output values were exact to the third decimal place. The difference in single precision accuracy occurs because the CDC system uses a 64 bit word length while the IBM system word length in single precision is only 32 bits. It was

decided that the IBM single precision accuracy was satisfactory.

B. COMPARISON WITH OTHER PROGRAMS

The FLC27 program was also tested for accuracy by using the wing planform and section data from a NACA 572 wing. The data were run on both the FLO27 program and the Douglas potential flow program [Ref. 1]. The data generated by both programs was compared to wind tunnel data for the NACA 572 wing [Ref. 8]. The results are presented in Fig. 5.1 as plots of lift coefficient versus angle-of-attack. The results show that for the NACA 572 wing the FLO27 program more accurately predicts the wing lift coefficient than does the Douglas program.

C. AE-4501 CLASS PROJECT

The final test phase was conducted by introducing the FLO27 program into the AE-4501 course as a class project. This was accomplished to determine student problems/comments concerning the data input program FLO27IN and to test an additional wing shape. The wing chosen for study was that of the A-7 airplane. The A-7 wing has a distinct leading edge notch at the approximate mid-span. When the planform geometry was run with the notch included the FLO27 program

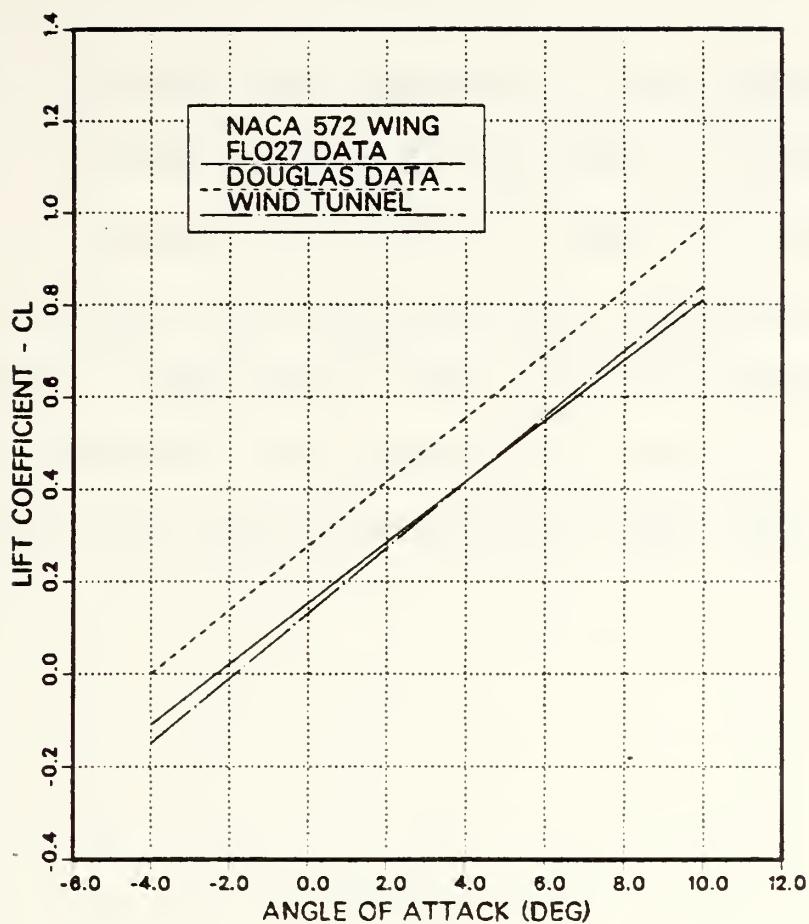


Figure 5.1. Program Calculated and Wind Tunnel Data

ran to completion but gave negative values for section and total induced drag coefficient. The value for the lift coefficient was low for the freestream Mach and angle-of-attack used. It was found that if the notch was

excluded from the wing geometry input data the program results were satisfactory both for induced drag and lift coefficient.

From the AE-4501 class experience it was determined that sharp wing planform discontinuities cannot be handled by the program. If however, the changes in shape are gradual, such as a wing glove, the program output appears to be satisfactory. Such was the case with the acceptance test case data where the wing geometry was that of the F-8 supercritical wing which incorporates a wing glove.

APPENDIX A

```
C This JCL routine allocates sufficient space on the mass
C storage system to store the entire tape contents
//JACK JOB (3266,0178), 'PASCHALL-2759', CLASS=A
//*MAIN ORG=NEGVM1.3266P
// EXEC PGM=IEFBR14
//DD1 DD UNIT=3330V,MSVGP=PUB4C,DISP=(NEW,CATLG),
// DSN=MSS.S3266.WFLOW.DATA,SPACE=(CYL,(16,4,2))
/*
//
```

```
C This JCL routine is used to transfer all tape files to
C a partitioned data set in the mass storage system
//JACK JOB (3266,0178), 'PASCHALL-2759', CLASS=J
//*MAIN ORG=NPGVM1.3266P
//COPY PROC FILE=,MEM=
// EXEC PGM=IEBGENER
//SYSPRINT DD SYSOUT=A
//SYSIN DD DUMMY
//SYSUT1 DD UNIT=3400-6,VCL=SER=WFLOW,DISP=(OLD,PASS),
// LABEL=(&FILE,BLP,,IN)
// DCB=(RECFM=F,BLKSIZE=80,DEN=3,OPTCD=Q)
//SYSUT2 DD DISP=(OLD,KEEP),
// DSN=MSS.S3266.WFLOW.SOURCE(&MEM),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=6400)
// PEND
// EXEC COPY,FILE=1,MEM=FLO27
// EXEC COPY,FILE=2,MEM=A411IN
// EXEC COPY,FILE=3,MEM=VWIN
// EXEC COPY,FILE=4,MEM=A411AO1
// EXEC COPY,FILE=5,MEM=INTERF
// EXEC COPY,FILE=6,MEM=A411PS
// EXEC COPY,FILE=7,MEM=A411P1
// EXEC COPY,FILE=8,MEM=A411P2
// EXEC COPY,FILE=9,MEM=COUPLE
// EXEC COPY,FILE=10,MEM=ITER
// EXEC COPY,FILE=11,MEM=DATAIN
// EXEC COPY,FILE=12,MEM=FINAL
// EXEC COPY,FILE=13,MEM=BOEB1
// EXEC COPY,FILE=14,MEM=CONTPLT
// EXEC COPY,FILE=15,MEM=CORDPLT
// EXEC COPY,FILE=16,MEM=STREPLT
//COPY2 PROC FILE=,MEM=,LRECL=80,BLK=6400
// EXEC PGM=IEBGENER
//SYSPRINT DD SYSOUT=A
//SYSIN DD DUMMY
//SYSUT1 DD UNIT=3400-6,VOL=SER=WFLOW,DISP=(OLD,PASS),
// LABEL=(&FILE,BLP,,IN)
// DCB=(RECFM=F,BLKSIZE=&LRECL,DEN=3,OPTCD=Q)
//SYSUT2 DD DISP=(OLD,KEEP),DSN=MSS.S3266.WFLOW.DATA(&MEM),
// DCB=(RECFM=FB,LRECL=&LRECL,BLKSIZE=&BLK)
// PEND
// EXEC COPY2,FILE=17,LRECL=150,BLK=6000,MEM=OUTF27
// EXEC COPY2,FILE=18,LRECL=150,BLK=6000,MEM=OUTIFC
// EXEC COPY2,FILE=19,LRECL=150,BLK=6000,MEM=OUT411L
// EXEC COPY2,FILE=20,LRECL=150,BLK=6000,MEM=OUT411U
/*
//
```


C This JCL routine moves all source code files from mass
 C storage to the MVS 004 disk which can be accessed by
 C entering GET MVS then following the screen instructions
 C to move source files to your disk. If you want to move
 C the data files to MVS 004 then change the word SOURCE
 C to DATA in the JCL program below.

```

//JACK JOB (3266,0178), 'FASCHALL-2759', CLASS=A
//*MAIN ORG=NPGVM1.3266P
// EXEC PGM=IEBCOPY
//SYSPRINT DD SYSOUT=A
//FROM DD DISP=SHR, DSN=MSS.S3266.WFLOW.SOURCE
//INTO DD UNIT=3350, VOL=SER=MVS004, DISP=(NEW,KEEP),
//      SPACE=(CYL,(16,4,10),RLSE), DSN=S3266.SOURCE
//SYSUT3 DD UNIT=SYSDA, SPACE=(CYL,(2,2))
//SYSUT4 DD UNIT=SYSDA, SPACE=(CYL,(2,2))
//SYSIN DD *
COPY OUTDD=INTC, INDD=FFCM
/*
//
  
```


APPENDIX B

LIBRARY OF AIRFOIL SECTION GEOMETRIES

- 0 = user input section coordinate data
- 1 = flat plate data
- 2 = symmetrical wing (11% thickness at 30% chord)
- 3 = supercritical wing (cambered, 12% thickness at 32% chord)
- 4 = NACA 24-30-0 (cambered, 12% thickness at 30% chord)
- 5 = F-14 wing (cambered, 9.5% thickness at 37% chord)
- 6 = A-7 wing (7 deg droop at 20% chord, 7% thickness at 43% chord)
- 7 = LISSAMAN 7769 Airfoil (cambered, 11% thickness at 30% chord)
- 8 = NACA 0010 (symmetrical, 10% thickness at 30% chord)
- 9 = NACA 0010-34 (symmetrical, 10% thickness at 40% chord)
- 10 = NACA 0010-35 (symmetrical, 10% thickness at 50% chord)
- 11 = NACA 0010-64 (symmetrical, 10% thickness at 40% chord)
- 12 = NACA 0010-66 (symmetrical, 10% thickness at 60% chord)
- 13 = NACA 16-009 (symmetrical, 9% thickness at 50% chord)
- 14 = NACA 63-010 (symmetrical, 10% thickness at 35% chord)
- 15 = NACA 63A010 (symmetrical, 10% thickness at 35% chord)
- 16 = NACA 64-010 (symmetrical, 10% thickness at 40% chord)
- 17 = NACA 64A010 (symmetrical, 10% thickness at 40% chord)
- 18 = NACA 65-010 (symmetrical, 10% thickness at 40% chord)
- 19 = NACA 65A010 (symmetrical, 10% thickness at 40% chord)
- 20 = NACA 66-010 (symmetrical, 10% thickness at 45% chord)

APPENDIX D

THIS APPENDIX PRESENTS THE FLG27 OUTPUT DATA PRODUCED FROM THE INPUT DATA OF THE PREVIOUS APPENDIX.

A46C MODIFIED FROM FLG27 OF ANTICNY JAMESON, CURRENT INSTALUTE THREE DIMENSIONAL WING ANALYSIS IN TRANSONIC FLOW USING FINITE VOLUME SCHEME
NACA 572 WING SECTION
FUSELAGE RAL

0.0
SWEEP
32.3275
CIHED
0.0

PROFILE AT Z = 0.0
TE ANGLE
16.0833
TE SLOPE
-0.0720
X SING
0.0024
Y SING
-0.0000

NL = 21, XF(NL) = 0.0

(XP,YP)

1.00000	-0.00130	0.95000	-0.00400	0.90000	-0.00820
0.60000	-0.02600	0.50000	-0.03200	0.40000	-0.03580
0.20000	-0.04220	0.15000	-0.04200	0.10000	-0.03750
0.03000	-0.02270	0.02000	-0.01680	0.01000	-0.01200
0.03000	0.00000	0.00250	0.00500	0.00500	0.00700
0.20000	0.02900	0.04000	0.03500	0.05000	0.04140
0.60000	0.07260	0.25000	0.07680	0.30000	0.07880
1.00000	0.00130	0.70000	0.05150	0.80000	0.03760

SECTION DEFINITION AT Z =		CHORD		THICKNESS RATIO		TWIST	
XLE	YLE	8.6000	8.6000	1.0000	1.0000	0.0	0.0
YMIN	JMIN	YMAX	YMAX	JMAX	JMAX	YDIF	YDIF
-4220E-01	10	7880E-01	7880E-01	33	33	.1210	.1210
SECTION DEFINITION AT Z =							
XLE	YLE	CHORD	CHORD	THICKNESS RATIO	THICKNESS RATIO	TWIST	TWIST
6.1307	0.0	6.4500	6.4500	1.0000	1.0000 <td>0.0</td> <td>0.0</td>	0.0	0.0
YMIN	JMIN	YMAX	YMAX	JMAX	JMAX	YDIF	YDIF
-4220E-01	10	7880E-01	7880E-01	33	33	.1210	.1210
SECTION DEFINITION AT Z =							
XLE	YLE	CHORD	CHORD	THICKNESS RATIO	THICKNESS RATIO	TWIST	TWIST
12.2614	0.0	4.3000	4.3000	1.0000	1.0000 <td>0.0</td> <td>0.0</td>	0.0	0.0
YMIN	JMIN	YMAX	YMAX	JMAX	JMAX	YDIF	YDIF
-4220E-01	10	7880E-01	7880E-01	33	33	.1210	.1210

SECTION CHARACTERISTICS

MACH NO	0.0	CL	
SPAN STATION	0.0	20238	
	3.87499	24033	
	7.74599	26515	
	11.62498	28127	
	15.49998	28695	
	19.37497	24168	

WING CHARACTERISTICS

MACH NO	0.0	CD	FCRM
	0.10000	-	.32534E-02
	0.25575	CM	ROLL
	-0.00467		.23919

ANG OF ATTACK

2.0000	CD	
71088E-02		
24623E-02		
48115E-02		
57074E-02		
65451E-02		
70588E-02		

ANG CF ATTACK

2.0000	CD	FRIC
10000E-01		ICN
CM	PITCH	
-	.33140	

L/D FORM
-78.612
L/D
37.

52

SECTION CHARACTERISTICS

MACH NO	0.1000	CL	22093	ANG GF ATTACK	2.0000
SPAN STATION	0.0	CL	24319	CM	10566
	1.93750		26053		10667
	3.87499		27508		10952
	5.81249		28683		11248
	7.74595		29643		11524
	9.68749		30359		11750
	11.62499		30863		11920
	13.56248		30746		11986
	15.45998		29141		11812
	17.43747		21866		10990
	19.37497				78297E-01

WING CHARACTERISTICS

MACH NO	0.1000	CL	22093	ANG GF ATTACK	2.0000
SPAN STATION	0.0	CL	24319	CD FRICTION	10000E-01
	1.93750		26053	CM PITCH	35963
	3.87499		27508		
	5.81249		28683		
	7.74595		29643		
	9.68749		30359		
	11.62499		30863		
	13.56248		30746		
	15.45998		29141		
	17.43747		21866		
	19.37497				


```

MAX RESIDUAL 0.13855E-02
-- 0.98673E-03
0.87373E-03
0.73407E-03
0.62240E-03
(CYCLE CONV TOLERANCE-05
0.8187
J 16 15 15 15 15
K 243333

```


SECTION CHARACTERISTICS

MACH NO	0.10000	CL	2236
YAW	0.0	CD	23679
SPAN	0.0	CD	24748
STATION	0.0	CD	25653
	0.0	CD	26526
	0.0	CD	27275
	0.0	CD	27957
	0.0	CD	28574
	0.0	CD	29139
	0.0	CD	29616
	0.0	CD	30522
	0.0	CD	30877
	0.0	CD	31151
	0.0	CD	31355
	0.0	CD	31168
	0.0	CD	30595
	0.0	CD	29369
	0.0	CD	26619
	0.0	CD	20055

WING CHARACTERISTICS

MACH NO	0.10000	CL	2236
YAW	0.0	CD	23679
SPAN	0.0	CD	24748
STATION	0.0	CD	25653
	0.0	CD	26526
	0.0	CD	27275
	0.0	CD	27957
	0.0	CD	28574
	0.0	CD	29139
	0.0	CD	29616
	0.0	CD	30522
	0.0	CD	30877
	0.0	CD	31151
	0.0	CD	31355
	0.0	CD	31168
	0.0	CD	30595
	0.0	CD	29369
	0.0	CD	26619
	0.0	CD	20055

A46C MODIFIED FROM FLC27 OF ANTCNY JAMESON, CCURANT INSTILUTE
THREE DIMENSIONAL WING ANALYSIS IN TRANSONIC FLOW USING FINITE VOLUME SCHEME
BOEING VERSION, PREPARED BY DR. HAI-CHOW CHEN STANDARD BOEING INPUT FORMAT
END OF CALCULATION

ANG OF ATTACK

ANG OF ATTACK	2.0000	CD	2236
	2.0000	CD	23679
	2.0000	CD	24748
	2.0000	CD	25653
	2.0000	CD	26526
	2.0000	CD	27275
	2.0000	CD	27957
	2.0000	CD	28574
	2.0000	CD	29139
	2.0000	CD	29616
	2.0000	CD	30522
	2.0000	CD	30877
	2.0000	CD	31151
	2.0000	CD	31355
	2.0000	CD	31168
	2.0000	CD	30595
	2.0000	CD	29369
	2.0000	CD	26619
	2.0000	CD	20055

ANG OF ATTACK

ANG OF ATTACK	2.0000	CD	2236
	2.0000	CD	23679
	2.0000	CD	24748
	2.0000	CD	25653
	2.0000	CD	26526
	2.0000	CD	27275
	2.0000	CD	27957
	2.0000	CD	28574
	2.0000	CD	29139
	2.0000	CD	29616
	2.0000	CD	30522
	2.0000	CD	30877
	2.0000	CD	31151
	2.0000	CD	31355
	2.0000	CD	31168
	2.0000	CD	30595
	2.0000	CD	29369
	2.0000	CD	26619
	2.0000	CD	20055

[illegible][illegible]

0.035734	-C.051941	0.043503	-0.177332	0.052008	-0.334910	0.061654	-0.435746
0.072512	-C.450552	0.084319	-0.411025	0.096972	-0.336700	0.110347	-0.435076
0.124444	-C.364866	0.139315	-0.332795	0.155014	-0.416500	0.171564	-0.444775
0.188567	-C.443092	0.207137	-0.443005	0.226132	-0.433916	0.245938	-0.442164
0.266561	-C.441034	0.288014	-0.439865	0.310732	-0.433819	0.333338	-0.437646
0.357204	-C.410349	0.381868	-0.435576	0.407327	-0.433260	0.433376	-0.433523
0.460617	-C.366049	0.488449	-0.435576	0.517071	-0.434501	0.546485	-0.433523
0.576692	-C.311980	0.607694	-0.435576	0.639486	-0.434501	0.672059	-0.433523
0.705395	-C.058370	0.739502	-0.435576	0.774388	-0.434501	0.810070	-0.433523
0.846511	-C.058370	0.883730	-0.435576	0.921712	-0.434501	0.960470	-0.433523
1.000000	-C.214168	0.000000	-0.000000	0.000000	-0.000000	0.000000	-0.000000

SPAN STATION = 1.93750
NO. CF DATA POINTS = 101

1.000000	C.235694	0.960452	0.206138	X/C	0.521777	CP	1.592654	X/C	0.883857	CF	1.592654
0.846730	C.100136	0.810396	0.077224	0.674065	0.774854	0.155583	0.002349	0.740105	0.740105	0.155583	
0.706152	C.012438	0.672598	0.002469	0.519055	0.640655	0.021899	0.002349	0.609054	0.609054	0.021899	
0.578298	C.027180	0.436282	0.002469	0.410261	0.510261	0.021899	0.002349	0.385015	0.385015	0.021899	
0.463050	-C.050332	0.250026	0.002469	0.313940	0.230322	0.021899	0.002349	0.291831	0.291831	0.021899	
0.360542	-C.123109	0.175832	0.002469	0.230322	0.159224	0.021899	0.002349	0.211358	0.211358	0.021899	
0.270527	-C.142549	0.114441	0.002469	0.159224	0.101106	0.021899	0.002349	0.143458	0.143458	0.021899	
0.193235	-C.192727	0.065638	0.002469	0.101106	0.055508	0.021899	0.002349	0.088501	0.088501	0.021899	
0.128543	-C.214849	0.030935	0.002469	0.055508	0.024413	0.021899	0.002349	0.046326	0.046326	0.021899	
0.076658	-C.210561	0.009182	0.002469	0.024413	0.006189	0.021899	0.002349	0.018956	0.018956	0.021899	
0.038378	-C.236647	0.003595	0.002469	0.006189	0.001189	0.021899	0.002349	0.003363	0.003363	0.021899	
0.013327	-C.255775	0.001704	0.002469	0.001189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.001528	-C.556264	0.000359	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.012560	-C.429114	0.003503	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.035734	-C.516314	0.084319	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.072512	-C.416798	0.139315	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.124444	-C.472197	0.207137	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.188567	-C.472197	0.288014	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.266561	-C.472197	0.381868	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.357204	-C.472197	0.488449	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.460617	-C.422580	0.576692	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.576692	-C.422580	0.672059	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.705395	-C.306606	0.810070	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
0.846511	-C.183974	0.960470	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
1.000000	-C.044431	0.000000	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	
	-C.215122	0.000000	0.002469	0.000189	0.000189	0.021899	0.002349	0.000177	0.000177	0.021899	

SPAN STATION = 2.90625
NO. CF DATA POINTS = 101

1.000000	C.236239	0.960492	0.207084	X/C	0.521777	CP	1.611711	X/C	0.883857	CF	1.611711
0.846730	C.102997	0.810396	0.077485	0.774854	0.774854	0.159673	0.002349	0.740105	0.740105	0.159673	
0.706152	C.029155	0.436282	0.002349	0.640641	0.640641	0.021899	0.002349	0.609077	0.609077	0.021899	

[illegible]

SPAN STATION = 3.87499
NO. OF DATA POINTS = 101

[illegible]

0.460617	-C.372240	0.488449	-0.356717	0.517071	-0.341032	0.546485	-0.32354
0.576692	-C.301548	0.607694	-0.272598	0.639466	-0.237831	0.672056	-0.20293
0.705355	-C.173943	0.739502	-0.150774	0.774388	-0.124863	0.810059	-0.08646
0.846511	-C.036027	0.883730	0.01485C	0.921712	0.068256	0.960470	0.14686
1.000000	-C.217029						

SPAN STATION = 4.84374
NO. CF DATA PCINTS = 101

1.000000	C.237192	0.960492	0.208446	0.521777	0.163078	0.883857	0.13065
0.846730	C.105858	0.810259	0.083923	0.774854	0.063487	0.740105	0.04536
0.706152	C.033375	0.672558	0.030518	0.640641	0.032970	0.609077	0.02342
0.578298	C.022889	0.548303	0.006676	0.519059	0.005567	0.490654	0.01353
0.463050	-C.018238	0.436282	0.001394	0.410261	-0.001367	0.391835	-0.00168
0.360542	-C.042721	0.336026	0.006760	0.330321	0.001524	0.291358	-0.01153
0.270527	-C.116851	0.250026	0.017327	0.230321	0.011972	0.211358	-0.02041
0.193235	-C.137934	0.175837	0.016517	0.159222	0.015863	0.143458	-0.01745
0.128548	-C.188053	0.114441	0.022075	0.101507	0.021910	0.088531	-0.01667
0.038050	-C.209305	0.030635	0.005722	0.055514	0.003351	0.046334	0.02277
0.013378	-C.261988	0.009184	0.032930	0.024315	0.045531	0.003362	0.55611
0.001528	C.495093	0.003555	0.065640	0.006159	0.639182	0.009017	0.28773
0.035512	C.174114	0.017041	0.049209	0.022008	0.325597	0.028618	0.10519
0.072444	-C.613255	0.043503	0.032975	0.096572	-0.050977	0.061694	-0.06085
0.128946	-C.481384	0.139316	0.058673	0.155014	0.455938	0.110347	0.52503
0.188946	-C.510275	0.288015	0.050740	0.226132	0.524044	0.175939	0.51726
0.266567	-C.445434	0.381869	0.042658	0.310273	0.481922	0.333338	0.44144
0.357205	-C.374505	0.488450	0.043587	0.407327	0.440835	0.433577	0.35107
0.460618	-C.301668	0.607694	0.032325	0.517071	0.342105	0.546485	0.32413
0.576692	-C.172896	0.739502	0.014966	0.639466	0.237831	0.672056	0.20293
0.705355	-C.034988	0.883730	0.001621	0.774388	0.068256	0.810059	0.08646
0.846511	-C.217983			0.921712		0.960470	
1.000000							

SPAN STATION = 5.81249
NO. CF DATA PCINTS = 101

1.000000	C.237192	0.960492	0.208991	0.521777	0.163620	0.883857	0.13160
0.846730	C.106812	0.810259	0.085422	0.774854	0.064850	0.740105	0.04673
0.706152	C.034877	0.672558	0.030518	0.640641	0.034332	0.609077	0.02352
0.578298	C.024796	0.548303	0.006588	0.519059	0.007570	0.490654	0.01445
0.463050	-C.016093	0.436282	0.001176	0.410261	-0.001144	0.391835	-0.00188
0.360542	-C.040318	0.336026	0.006504	0.330321	0.008819	0.291358	-0.01160
0.270527	-C.113904	0.250026	0.014236	0.230321	0.012119	0.211358	-0.01356
0.193235	-C.134451	0.175837	0.016536	0.159222	0.015345	0.143458	-0.01165
0.128548	-C.183433	0.114441	0.021196	0.101507	0.021533	0.088531	0.02277
0.038050	-C.209305	0.030635	0.005722	0.055514	0.003351	0.046334	0.55611
0.013378	-C.261988	0.009184	0.032930	0.024315	0.639182	0.009017	0.28773
0.001528	C.495093	0.003555	0.049209	0.022008	0.325597	0.028618	0.10519
0.035512	C.174114	0.017041	0.032975	0.096572	-0.050977	0.061694	-0.06085
0.072444	-C.613255	0.043503	0.058673	0.155014	0.455938	0.110347	0.52503
0.128946	-C.481384	0.139316	0.050740	0.226132	0.524044	0.175939	0.51726
0.188946	-C.510275	0.288015	0.042658	0.310273	0.481922	0.333338	0.44144
0.266567	-C.445434	0.381869	0.043587	0.407327	0.440835	0.433577	0.35107
0.357205	-C.374505	0.488450	0.043587	0.517071	0.342105	0.546485	0.32413
0.460618	-C.301668	0.607694	0.014966	0.639466	0.237831	0.672056	0.20293
0.576692	-C.172896	0.739502	0.001621	0.774388	0.068256	0.810059	0.08646
0.705355	-C.034988	0.883730	0.001621	0.921712	0.068256	0.960470	0.14686
0.846511	-C.217983						
1.000000							

CP	X/C	CP	X/C	CP	X/C	CP	X/C
0	921778	0	1641648	0	883857	0	883857
0	7748429	0	1663478	0	7401077	0	7401077
0	6406459	0	0004385	0	6090777	0	6090777
0	5190559	0	0007685	0	4906515	0	4906515
0	4103241	0	0008359	0	391831	0	391831
0	3130321	0	0018463	0	2113987	0	2113987
0	2302246	0	0019478	0	1434571	0	1434571
0	1592106	0	0019480	0	0885014	0	0885014
0	054313	0	0019707	0	0832646	0	0832646
0	0243188	0	0043759	0	0186256	0	0186256
0	0061	0	0063574	0	0035563	0	0035563
0	06186	0	0056692	0	0090187	0	0090187
0	022308	0	0056627	0	0261654	0	0261654
0	0529722	0	0053355	0	110564	0	110564
0	096972	0	0053964	0	171564	0	171564
0	001314	0	0053964	0	245339	0	245339
0	2261217	0	0044765	0	33338	0	33338
0	3107372	0	0044743	0	4335765	0	4335765
0	407072	0	0033565	0	546485	0	546485
0	517072	0	0022436	0	672059	0	672059
0	6394388	0	0012696	0	8104770	0	8104770
0	774712	0	000	0	9604770	0	9604770
0	521712	0	000	0	5604770	0	5604770

[illegible]

0.0357734	-0.0246650	0.0433203	-0.0380653	0.0529712	-0.0557601	0.0616555	-0.06571
0.0072512	-0.0665551	0.0084320	-0.0360560	0.0096972	-0.0554184	0.0110348	-0.0556149
0.0188944	-0.0517351	0.0130713	-0.0535581	0.0155014	-0.0547031	0.0171564	-0.0540188
0.0124467	-0.0554093	0.0207113	-0.0547911	0.0226127	-0.0547361	0.0245939	-0.0540082
0.0266567	-0.0532244	0.0338015	-0.0541803	0.0310232	-0.0500321	0.0333338	-0.0540171
0.0357205	-0.0460454	0.0381869	-0.0440052	0.0407327	-0.0420366	0.0433577	-0.0430332
0.0460618	-0.0383905	0.0488449	-0.0366620	0.0517011	-0.0434930	0.0546485	-0.0430478
0.0705395	-0.0306938	0.0676542	-0.0276668	0.0639486	-0.0240718	0.0672056	-0.0208611
0.0846511	-0.0175008	0.0739550	-0.0151277	0.0774388	-0.0124948	0.0810059	-0.0144531
1.0000000	-0.0219890	0.0883750	-0.0116212	0.0821712	-0.0069618	0.0960470	-0.0144531

SPAN STATION = 5.68749
 NO. OF DATA POINTS = 101

1.0000000	0.0800730	0.0560492	0.0237601	0.0103396	0.0017777	0.083857	0.03310
0.0706152	-0.0386192	0.0610359	-0.0386192	0.0774064	-0.0673302	0.0740105	-0.0495594
0.0578297	-0.0255660	0.0548303	-0.0255660	0.0519059	-0.0386922	0.0609077	-0.0301514
0.0463090	-0.0324855	0.0436282	-0.0324855	0.0410261	-0.0209923	0.0490653	-0.0136445
0.0370542	-0.0121220	0.0350026	-0.0121220	0.0330321	-0.0066893	0.0391398	-0.0053868
0.0193235	-0.0165422	0.0175841	-0.0165422	0.0159224	-0.0106134	0.0211357	-0.0147311
0.0128542	-0.0174769	0.0144417	-0.0174769	0.0130321	-0.0133319	0.0143451	-0.0124492
0.0076658	-0.0308305	0.0065637	-0.0308305	0.0111067	-0.0177094	0.0088501	-0.0147311
0.0038050	-0.0457029	0.0030635	-0.0457029	0.0055572	-0.0174651	0.0046334	-0.0128430
0.0013378	-0.0399155	0.0009184	-0.0399155	0.0024312	-0.0148501	0.0018626	-0.0058240
0.0001528	-0.0331061	0.0003625	-0.0331061	0.0006186	-0.0063022	0.0003362	-0.0011337
0.0012560	-0.0149866	0.0017041	-0.0149866	0.0061555	-0.0038721	0.0009017	-0.0017706
0.0035734	-0.0257440	0.0043503	-0.0257440	0.0223088	-0.0056767	0.0061654	-0.0017806
0.0124444	-0.0523539	0.0139315	-0.0523539	0.0969722	-0.0054909	0.0110347	-0.0055514
0.0188546	-0.0555109	0.0207137	-0.0555109	0.1550141	-0.0056267	0.0171564	-0.0055514
0.0266567	-0.0466169	0.0281868	-0.0466169	0.2261311	-0.0054921	0.0245939	-0.0048397
0.0357204	-0.0363367	0.0381868	-0.0363367	0.3102377	-0.0052283	0.0333516	-0.0043193
0.0460618	-0.0308335	0.0488449	-0.0308335	0.4070371	-0.0054341	0.0436485	-0.0039733
0.0576922	-0.0308335	0.0607694	-0.0308335	0.5170486	-0.0052283	0.0546056	-0.0039733
0.0705395	-0.0175817	0.0739550	-0.0175817	0.6394388	-0.0054341	0.0672056	-0.0039733
0.0846511	-0.0035465	0.0883750	-0.0035465	0.774712	-0.0052283	0.0810059	-0.0039733
1.0000000	-0.0219890	0.0883750	-0.0035465	0.921712	-0.0052283	0.0960470	-0.0039733

SPAN STATION = 10.65624
 NO. OF DATA POINTS = 101

1.0000000	0.0237601	0.0560492	0.0084320	0.083857	0.03310
0.0846730	-0.0386192	0.0610359	-0.0386192	0.0740105	-0.0495594
0.0706152	-0.0255660	0.0548303	-0.0255660	0.0609077	-0.0301514

0.460617 -C.385346 0.488450 -0.371584 0.517071 0.546485 -0.333443
 0.576692 -C.310566 0.607694 -0.279852 0.639486 0.672056 -0.020707
 0.705355 -C.176945 0.739502 -0.152886 0.774388 0.810059 -0.008703
 0.846511 -C.035729 0.883730 0.016212 0.921712 0.960470 0.14572
 1.000000 -C.220435

SPAN STATION = 12.59373
 NO. OF DATA PCINTS = 101

X/C	CP	X/C	CP	X/C	CP	X/C	CP
1.000000	C.237601	0.560491	0.209400	0.521777	0.165122	0.883857	0.03351
0.846730	C.105264	0.810396	0.088283	0.774854	0.068256	0.740105	0.003564
0.706151	C.035646	0.672957	0.037193	0.640641	0.0039646	0.609077	0.000000
0.578298	C.031063	0.548303	0.015259	0.519059	0.0001848	0.490653	0.000000
0.463050	C.007391	0.436282	0.002622	0.410261	0.00075204	0.385015	0.000000
0.360542	C.028993	0.336848	0.005760	0.339321	0.00094720	0.291831	0.000000
0.270527	C.098203	0.250026	0.014300	0.230321	0.00168434	0.211358	0.000000
0.193235	C.114262	0.175832	0.013206	0.159222	0.00122355	0.143458	0.000000
0.128543	C.155594	0.114441	0.017784	0.101106	0.00122341	0.088501	0.000000
0.076658	C.160839	0.065638	0.013206	0.055231	0.00191822	0.046334	0.000000
0.038050	C.031258	0.030635	0.006730	0.024313	0.00150136	0.018626	0.000000
0.013378	C.326838	0.009184	0.035087	0.006119	0.00510760	0.003362	0.000000
0.001528	C.645043	0.000362	0.670161	0.001166	0.0315208	0.000917	0.000000
0.012560	C.092098	0.017041	0.031558	0.022359	0.01105927	0.028618	0.000000
0.035734	C.278098	0.043503	0.415070	0.052008	0.05918573	0.061654	0.000000
0.072512	C.658209	0.084320	0.540235	0.095972	0.05664883	0.110347	0.000000
0.124445	C.538341	0.139315	0.559677	0.155014	0.05761989	0.171564	0.000000
0.188944	C.571030	0.207137	0.563745	0.226131	0.05556799	0.245938	0.000000
0.266567	C.545323	0.288014	0.530192	0.302273	0.05115533	0.333338	0.000000
0.357204	C.465932	0.381868	0.478738	0.407326	0.0428276	0.433576	0.000000
0.460617	C.390444	0.488449	0.372514	0.517071	0.03546313	0.546485	0.000000
0.576692	C.311102	0.607694	0.280244	0.639486	0.02243723	0.672056	0.000000
0.705355	C.177034	0.739502	0.152920	0.774388	0.01261775	0.810059	0.000000
0.846511	C.035524	0.883730	0.016212	0.921712	0.00070163	0.960470	0.000000
1.000000	C.220844	0.883730	0.000000	0.521777	0.000000	0.000000	0.000000

SPAN STATION = 13.56248
 NO. OF DATA PCINTS = 101

X/C	CP	X/C	CP	X/C	CP	X/C	CP
1.000000	C.237601	0.960492	0.209400	0.921777	0.165122	0.883857	0.03351
0.846730	C.109264	0.810396	0.088283	0.774854	0.068256	0.740105	0.003564
0.706152	C.033964	0.672958	0.037193	0.640642	0.0039646	0.609077	0.000000
0.578298	C.031063	0.548303	0.015804	0.519059	0.0001550	0.490654	0.000000
0.463050	C.007178	0.436283	0.002418	0.410261	0.00074548	0.385015	0.000000
0.360542	C.028551	0.336847	0.002060	0.339321	0.00093673	0.291831	0.000000
0.270527	C.097368	0.250026	0.005684	0.230321	0.00166706	0.211358	0.000000
0.193235	C.112951	0.175832	0.014148	0.159224	0.00119856	0.143458	0.000000
0.128542	C.153542	0.114441	0.012989	0.101106	0.000000	0.088501	0.000000
0.076658	C.160839	0.065638	0.006730	0.055231	0.000000	0.046334	0.000000
0.038050	C.031258	0.030635	0.003508	0.024313	0.000000	0.018626	0.000000
0.013378	C.326838	0.009184	0.035087	0.006119	0.000000	0.003362	0.000000
0.001528	C.645043	0.000362	0.670161	0.001166	0.000000	0.000917	0.000000
0.012560	C.092098	0.017041	0.031558	0.022359	0.000000	0.028618	0.000000
0.035734	C.278098	0.043503	0.415070	0.052008	0.000000	0.061654	0.000000
0.072512	C.658209	0.084320	0.540235	0.095972	0.000000	0.110347	0.000000
0.124445	C.538341	0.139315	0.559677	0.155014	0.000000	0.171564	0.000000
0.188944	C.571030	0.207137	0.563745	0.226131	0.000000	0.245938	0.000000
0.266567	C.545323	0.288014	0.530192	0.302273	0.000000	0.333338	0.000000
0.357204	C.465932	0.381868	0.478738	0.407326	0.000000	0.433576	0.000000
0.460617	C.390444	0.488449	0.372514	0.517071	0.000000	0.546485	0.000000
0.576692	C.311102	0.607694	0.280244	0.639486	0.000000	0.672056	0.000000
0.705355	C.177034	0.739502	0.152920	0.774388	0.000000	0.810059	0.000000
0.846510	C.035524	0.883730	0.016212	0.921712	0.000000	0.960470	0.000000
1.000000	C.220844	0.883730	0.000000	0.521777	0.000000	0.000000	0.000000

0.076658	0.157682	0.065638	-0.174241	0.05557	-0.158379	0.046334	-0.128275
0.038051	0.026882	0.030635	0.035230	0.024313	0.195637	0.018626	0.128275
0.001337	0.331745	0.009184	0.552316	0.061138	0.050517	0.003596	0.053700
0.001522	0.050951	0.000365	0.695614	0.0	0.050999	0.000363	0.054192
0.001560	0.396184	0.003555	0.704344	0.06187	0.031307	0.009017	0.022558
0.035734	0.085831	0.043503	0.205484	0.022359	0.116936	0.028618	0.070411
0.072512	0.203761	0.084320	0.209894	0.052008	0.198039	0.061655	0.053712
0.128546	0.541815	0.139316	0.632945	0.096912	0.579206	0.110347	0.053712
0.188546	0.573644	0.207137	0.661767	0.155613	0.618558	0.245939	0.053712
0.266567	0.471043	0.381868	0.549572	0.226124	0.542893	0.333338	0.053712
0.357205	0.350802	0.407326	0.729772	0.407326	0.425469	0.433577	0.053712
0.460617	0.310923	0.684550	0.779444	0.517071	0.345344	0.546485	0.053712
0.576693	0.176498	0.739503	0.152324	0.774388	0.225572	0.672059	0.053712
0.846511	0.034835	0.683730	0.017166	0.521712	0.070572	0.810059	0.053712
1.000000	0.22138	0.0	0.0	0.0	0.0	0.960470	0.053712

SPAN STATION = 14.53123
NO. CF DATA POINTS = 101

1.084673	0.238146	0.810396	0.094592	0.774877	0.164577	0.883857	0.130103
0.706152	0.035101	0.672558	0.033678	0.640642	0.039101	0.740105	0.130103
0.578298	0.031063	0.548304	0.015256	0.519059	0.000345	0.690654	0.030822
0.360543	0.007331	0.436282	0.002563	0.410261	0.001633	0.385015	0.001021
0.270523	0.028517	0.336848	0.019471	0.330321	0.074347	0.291398	0.005016
0.128543	0.096951	0.250226	0.056271	0.239225	0.165479	0.143458	0.016019
0.076658	0.121166	0.144411	0.128268	0.101108	0.118000	0.088502	0.015042
0.038050	0.152210	0.030635	0.171330	0.024313	0.152210	0.046334	0.015042
0.013378	0.023501	0.009184	0.039850	0.0	0.080362	0.003556	0.025531
0.001522	0.352466	0.003555	0.660750	0.06187	0.092726	0.009017	0.053712
0.035734	0.390460	0.043503	0.664950	0.022008	0.121321	0.028618	0.027104
0.072512	0.881227	0.084320	0.651868	0.096912	0.073703	0.110347	0.053712
0.128546	0.707774	0.139316	0.652205	0.155613	0.581369	0.171564	0.053712
0.188546	0.544288	0.207137	0.652205	0.226124	0.633694	0.245939	0.053712
0.266567	0.371377	0.381868	0.549333	0.407326	0.513341	0.333577	0.053712
0.357205	0.470919	0.407326	0.718574	0.517071	0.425469	0.433577	0.053712
0.460617	0.305646	0.684550	0.150774	0.639486	0.345344	0.546485	0.053712
0.576693	0.174958	0.739503	0.017166	0.774388	0.225572	0.672059	0.053712
0.846511	0.034342	0.683730	0.017166	0.521712	0.070572	0.810059	0.053712
1.000000	0.22234	0.0	0.0	0.0	0.0	0.960471	0.053712

SPAN NO. OF DATA PCINTS = 15.499998

NO.	X/C	CP	X/C	CP	X/C	CP	X/C	CP
1	0.00000	0.238146	0.560492	0.209400	0.521777	0.164577	0.883857	0.44559
0	0.846730	0.108310	0.8102396	0.08735831	0.774854	0.0367302	0.740105	0.043559
0	0.706152	0.038692	0.6728398	0.0335831	0.640641	0.0038692	0.609077	0.003669
0	0.578297	0.030109	0.548303	0.0148504	0.5190241	0.000715	0.490653	0.000890
0	0.463090	0.008013	0.436287	0.002597	0.410241	0.002350	0.385015	0.001093
0	0.360542	0.025208	0.335026	0.005683	0.339940	0.007494	0.291831	0.005072
0	0.270527	0.097488	0.250026	0.005683	0.230322	0.009361	0.211358	0.005595
0	0.193235	0.112534	0.175831	0.012822	0.159224	0.016569	0.143458	0.012592
0	0.128543	0.152085	0.114440	0.012822	0.101105	0.011792	0.088501	0.012592
0	0.076658	0.154674	0.065637	0.017054	0.055507	0.019986	0.046334	0.012592
0	0.038050	0.222079	0.030634	0.040407	0.024313	0.059398	0.018626	0.025586
0	0.013378	0.336511	0.005184	0.040407	0.006188	0.059398	0.003556	0.025586
0	0.001527	0.524449	0.003622	0.067300	0.006188	0.059398	0.003556	0.025586
0	0.001528	0.384194	0.003595	0.067300	0.006188	0.059398	0.003556	0.025586
0	0.012528	0.768399	0.013741	0.030964	0.006188	0.059398	0.003556	0.025586
0	0.035734	0.291816	0.013741	0.030964	0.006188	0.059398	0.003556	0.025586
0	0.072212	0.710564	0.084319	0.042471	0.052097	0.060582	0.061654	0.027128
0	0.124444	0.545561	0.139315	0.056211	0.155014	0.058208	0.171564	0.058341
0	0.188545	0.545561	0.207137	0.056211	0.226131	0.056265	0.245539	0.055126
0	0.266567	0.545561	0.288015	0.053111	0.310273	0.051791	0.333338	0.045071
0	0.357204	0.468667	0.381869	0.044714	0.407071	0.032604	0.433576	0.030512
0	0.460617	0.387141	0.488449	0.036876	0.517071	0.035043	0.546485	0.030512
0	0.576692	0.306223	0.607654	0.027515	0.639465	0.023842	0.672056	0.020189
0	0.705395	0.171619	0.739502	0.014755	0.774338	0.002092	0.810059	0.001888
0	0.846511	0.030816	0.883730	0.002057	0.921712	0.001739	0.960470	0.001554
1	0.00000	0.223296	0.883730	0.002057	0.921712	0.001739	0.960470	0.001554

SPAN NO. OF DATA PCINTS = 16.46472

NO.	X/C	CP	X/C	CP	X/C	CP	X/C	CP
1	0.00000	0.237192	0.560491	0.208037	0.521777	0.163078	0.883857	0.44119
0	0.846730	0.106812	0.8102396	0.085831	0.774854	0.065804	0.740105	0.044222
0	0.706152	0.037193	0.6728398	0.034877	0.640641	0.003719	0.609077	0.003719
0	0.578297	0.029155	0.548303	0.013335	0.5190241	0.001754	0.490653	0.001922
0	0.463090	0.009026	0.436287	0.004257	0.410241	0.003363	0.385015	0.001192
0	0.360542	0.030160	0.335026	0.005349	0.339940	0.007580	0.291831	0.005156
0	0.270527	0.098297	0.250026	0.014139	0.230322	0.009442	0.211358	0.005095
0	0.193235	0.132443	0.175831	0.012855	0.159224	0.016619	0.143458	0.012036
0	0.128543	0.154461	0.114440	0.017006	0.101105	0.018122	0.088501	0.012730
0	0.076658	0.221126	0.065635	0.040953	0.055507	0.020817	0.046334	0.025059
0	0.038050	0.336919	0.030635	0.065398	0.024313	0.059398	0.018626	0.025059
0	0.013378	0.514966	0.005185	0.039546	0.006188	0.059398	0.003556	0.045045
0	0.001527	0.777248	0.003622	0.039546	0.006188	0.059398	0.003556	0.045045
0	0.001528	0.387141	0.003595	0.039546	0.006188	0.059398	0.003556	0.045045
0	0.012528	0.777248	0.013741	0.039546	0.006188	0.059398	0.003556	0.045045
0	0.035734	0.291816	0.013741	0.039546	0.006188	0.059398	0.003556	0.045045
0	0.072212	0.710564	0.084319	0.056211	0.155014	0.058208	0.171564	0.058341
0	0.124444	0.545561	0.207137	0.056211	0.226131	0.056265	0.245539	0.055126
0	0.188545	0.545561	0.288015	0.053111	0.310273	0.051791	0.333338	0.045071
0	0.266567	0.468667	0.381869	0.044714	0.407071	0.032604	0.433576	0.030512
0	0.357204	0.387141	0.488449	0.036876	0.517071	0.035043	0.546485	0.030512
0	0.460617	0.306223	0.607654	0.027515	0.639465	0.023842	0.672056	0.020189
0	0.576692	0.171619	0.739502	0.014755	0.774338	0.002092	0.810059	0.001888
0	0.705395	0.030816	0.783730	0.002057	0.921712	0.001739	0.960470	0.001554
0	0.846511	0.030816	0.883730	0.002057	0.921712	0.001739	0.960470	0.001554
1	0.00000	0.223296	0.883730	0.002057	0.921712	0.001739	0.960470	0.001554

0.035734	-C.290532	0.0433503	-0.47118	0.052972	-0.04016	0.061654	-0.01178
0.072512	-C.708725	0.0843320	-0.242985	0.096972	0.065739	0.110347	0.054009
0.124444	-C.543543	0.139316	-0.056389	0.155014	-0.057946	0.171564	0.058050
0.188545	-C.572247	0.207137	-0.056392	0.226132	-0.053825	0.245939	0.055296
0.266567	-C.542257	0.288015	-0.052609	0.310237	-0.056410	0.333338	0.048501
0.357265	-C.462890	0.380210	-0.044706	0.407376	-0.041953	0.433576	0.035539
0.460617	-C.380210	0.488449	-0.036170	0.517071	-0.033263	0.546485	0.032333
0.576692	-C.255079	0.607694	-0.026810	0.639485	-0.023158	0.672056	0.019529
0.705335	-C.165335	0.735502	-0.014160	0.774388	-0.011538	0.810059	0.017681
0.846511	-C.022886	0.883730	-0.002479	0.921712	-0.007724	0.960470	0.015599
1.000000	-C.022520						

SPAN OF DATA = 17.43747
NO. OF POINTS = 101

1.000000	-C.235285	0.0960492	-0.065335	0.052177	-0.060762	0.083857	-0.02833
0.846730	-C.103542	0.810358	-0.208201	0.774854	0.162534	0.740105	0.12536
0.706151	-C.034332	0.672958	-0.022014	0.649642	-0.034877	0.609054	0.04387
0.578090	-C.026703	0.548303	-0.011442	0.519059	-0.035422	0.490654	-0.01156
0.463050	-C.010550	0.436283	-0.005472	0.410241	-0.007705	0.385015	-0.00528
0.360542	-C.031471	0.336848	-0.009921	0.313940	-0.009617	0.291831	-0.00589
0.270527	-C.095693	0.250025	-0.014368	0.230222	-0.012185	0.211358	-0.01301
0.193542	-C.115424	0.175441	-0.011319	0.159226	-0.011738	0.143458	-0.01385
0.126658	-C.158429	0.105638	-0.017402	0.101108	-0.015735	0.088501	-0.01350
0.076050	-C.025690	0.063635	-0.003527	0.055513	-0.011946	0.046334	-0.01250
0.038078	-C.030244	0.030635	-0.005421	0.024318	-0.005878	0.018626	-0.00514
0.013528	-C.043321	0.009185	-0.003489	0.006186	-0.005495	0.000563	-0.00490
0.001528	-C.037275	0.003595	-0.003489	0.00186	-0.002757	0.00017	-0.00189
0.012560	-C.072070	0.017041	-0.004286	0.022008	-0.005095	0.028694	-0.00618
0.072514	-C.091313	0.084319	-0.004387	0.096972	-0.005714	0.110347	-0.00709
0.124444	-C.073880	0.135315	-0.004552	0.155014	-0.005958	0.171564	-0.00547
0.188546	-C.053245	0.207137	-0.004552	0.226132	-0.005713	0.245939	-0.00540
0.266567	-C.052903	0.288014	-0.004387	0.310237	-0.004921	0.333338	-0.00470
0.357265	-C.044796	0.380210	-0.004387	0.407376	-0.004240	0.433577	-0.00385
0.460617	-C.036489	0.488450	-0.004240	0.517071	-0.003205	0.546485	-0.00354
0.576692	-C.028387	0.607654	-0.003546	0.639486	-0.002184	0.672056	-0.00309
0.705335	-C.015218	0.735503	-0.001301	0.774388	-0.001081	0.810059	-0.00164
0.846511	-C.022465	0.883730	-0.000000	0.921712	-0.001062	0.960470	-0.00153
1.000000							

SPAN OF DATA = 18.40622
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1.000000	-C.224658	0.0960494	-0.195639	0.052177	-0.064972	0.083859	-0.02130
0.846732	-C.093051	0.810358	-0.072479	0.774855	0.052997	0.740107	0.05583
0.706153	-C.025340	0.672999	-0.002343	0.640643	-0.002670	0.609078	-0.00272

SPAN ST ATION = 19.37497
NO. CF DATA PGINTS = 101

0.578299	C.020027	0.548304	0.005313	0.519100	-0.008821	0.490655	-0.001611
0.463090	C.014509	0.436283	0.009060	0.410261	0.007357	0.385016	0.001502
0.360543	C.032272	0.336848	0.005458	0.313941	0.007597	0.291832	0.001502
0.270237	C.009728	0.250026	0.003807	0.230322	0.001619	0.211358	0.001547
0.193253	C.011074	0.175832	0.001238	0.159224	0.001134	0.143458	0.001245
0.128543	C.014752	0.114440	0.001606	0.101106	0.001474	0.088501	0.001245
0.076658	C.008437	0.065638	0.001892	0.055507	0.001746	0.046334	0.001245
0.038050	C.033933	0.030635	0.004047	0.024313	0.005517	0.018626	0.001245
0.001527	C.036607	0.009184	0.009376	0.006118	0.005677	0.003562	0.001245
0.001528	C.036607	0.009376	0.009376	0.006118	0.005677	0.003562	0.001245
0.012560	C.009727	0.017040	0.004542	0.061817	0.003020	0.009017	0.001245
0.035734	C.025705	0.043503	0.008491	0.022308	0.005662	0.028618	0.001245
0.072512	C.062254	0.084319	0.003601	0.052008	0.005541	0.061654	0.001245
0.124444	C.050391	0.139316	0.006013	0.096912	0.005351	0.110347	0.001245
0.188946	C.052671	0.207138	0.005173	0.155014	0.005110	0.171564	0.001245
0.266567	C.049253	0.288015	0.004757	0.226132	0.005583	0.245939	0.001245
0.357205	C.041233	0.381869	0.003906	0.310732	0.003699	0.333333	0.001245
0.460619	C.033228	0.488459	0.003149	0.401701	0.002978	0.446486	0.001245
0.576693	C.025703	0.607695	0.002282	0.517012	0.001943	0.572057	0.001245
0.705356	C.011346	0.739504	0.001145	0.639487	0.000819	0.681061	0.001245
0.846512	C.001087	0.883731	0.000348	0.774389	0.000106	0.810061	0.001245
1.000000	C.021893	0.000000	0.000000	0.521714	0.000000	0.960473	0.001245

1.000000	C.155040	0.960490	0.140190	0.521719	0.105858	0.883856	0.081066
0.846132	C.061987	0.810397	0.145361	0.774855	0.129556	0.740106	0.115806
0.706153	C.006267	0.672999	0.002861	0.640643	0.020340	0.609078	0.001245
0.463090	C.003576	0.436283	0.001474	0.519100	0.002604	0.490654	0.001245
0.360543	C.003212	0.336848	0.000655	0.410261	0.000751	0.385016	0.001245
0.270237	C.004705	0.250026	0.002335	0.230322	0.000909	0.211358	0.001245
0.193253	C.010842	0.175832	0.001278	0.159224	0.001452	0.143458	0.001245
0.128543	C.013504	0.114440	0.001105	0.101106	0.001210	0.088501	0.001245
0.076658	C.009741	0.065638	0.001724	0.055507	0.001779	0.046334	0.001245
0.038050	C.028337	0.030635	0.003622	0.024313	0.004587	0.018626	0.001245
0.001527	C.025340	0.009184	0.003283	0.006118	0.004208	0.003562	0.001245
0.001528	C.025340	0.009184	0.003283	0.006118	0.004208	0.003562	0.001245
0.012560	C.003528	0.017041	0.002023	0.061817	0.001369	0.009017	0.001245
0.035734	C.005598	0.043503	0.003357	0.022308	0.001404	0.028618	0.001245
0.072512	C.005598	0.084319	0.003357	0.052008	0.001404	0.061654	0.001245
0.124444	C.005598	0.139316	0.003357	0.096912	0.001404	0.110347	0.001245
0.188946	C.005598	0.207138	0.003357	0.155014	0.001404	0.171564	0.001245
0.266567	C.005598	0.288015	0.003357	0.226132	0.001404	0.245939	0.001245
0.357205	C.005598	0.381869	0.003357	0.310732	0.001404	0.333333	0.001245
0.460619	C.005598	0.488459	0.003357	0.401701	0.001404	0.446486	0.001245
0.576693	C.005598	0.607695	0.003357	0.517012	0.001404	0.572057	0.001245
0.705356	C.005598	0.739504	0.003357	0.639487	0.001404	0.681061	0.001245
0.846512	C.005598	0.883731	0.003357	0.774389	0.001404	0.810061	0.001245
1.000000	C.030170	0.000000	0.000000	0.401714	0.000000	0.960473	0.001245

0.460619	-C.245829	0.488450	-0.239440	0.517072	-0.229495	0.546486	-0.21668
0.576693	-C.204904	0.607655	-0.186239	0.639487	-0.163666	0.672057	-0.14168
0.705356	-C.124829	0.739503	-0.112534	0.774389	-0.097547	0.810060	-0.07234
0.846512	-C.038530	0.883731	-0.006437	0.921712	0.025749	0.960469	0.007570
1.000000	C.142642						

APPENDIX E

THIS APPENDIX PRESENTS THE SOURCE CODE FOR THE POTENTIAL FLOW PROGRAM FLO27.

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*****FLO27*****9/12/83*****
*****THREE DIMENSIONAL WING ANALYSIS IN TRANSONIC FLOW USING
*****FINITE VOLUME SCHEME WITH SHEARED PARABOLIC COORDINATES
*****PROGRAMMED BY ANTONY JAMESON, JANUARY-APRIL 1977
*****
*****THE BEING VERSION OF FLO27 WAS PREPARED BY DR. HAI-CHOW
*****CHEN WITH THE FOLLOWING MODIFICATIONS
*****1) TEMPORARY STORAGE OF THE LARGE CORE MEMORY REQUIREMENTS
*****HAS BEEN IMPLEMENTED TO REDUCE THE COMPUTING COSTS
*****BY BUFFERING DATA IN AND OUT OF CORE.
*****
*****2) STANDARD BOEING INPUT FORMAT FOR THE WING SECTION
*****HAS BEEN USED.
*****
*****3) SUBPROGRAM BLIN HAS BEEN IMPLEMENTED TO ADD THE
*****DISPLACEMENT THICKNESS TO THE ORIGINAL WING SECTIONS
*****
*****4) WING SECTION LEADING EDGE SINGULAR POINT IS FOUND BY
*****COMPUTING THE FOCUS OF A PARABOLA BY 2N+1 POINTS
*****LEAST-SQUARE FIT CENTERED AT THE LEADING EDGE POINT.
*****N IS SUPPLIED BY THE USER THROUGH INPLT CARD.
*****
*****5) TRAILING EDGE CLOSURE ANGLE AND BISECTOR SLOPE ARE
*****COMPUTED BASED ON BACKWARD DIFFERENCE.
*****
*****6) OPTION FOR PRINTER-PLOTTING OF THE UNWRAPPED
*****WING SECTIONS IS AVAILABLE
*****
*****THE FOLLOWING FILES ARE USED TO EXECUTE FLO27. SOME OF THESE
*****FILES ARE USED SUBSEQUENTLY IN OTHER MODULES OF THE VISCOUS/
*****INVISCID INTERACTIVE WING SYSTEM
*****
*****FILE1 IS USED TO BUFFER DATA IN AND OUT OF CORE
*****
*****FILE2 IS USED TO BUFFER DATA IN AND OUT OF CORE
*****
*****FILE3 IS USED TO BUFFER DATA IN AND OUT OF CORE
*****

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CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
FILE4 IS USED TO READ IN THE VELOCITY PCTENTIAL
GENERATED PREVIOUSLY

FILE8 IS WRITTEN FOR DATA TRANSFER TO BCEING
TUREULENT BCUNCARY LAYER PROGRAM A411.

FILE9 IS USED TO SAVE SECTION SURFACE PRESSURE
AGAINST X/C.

FILE10 IS USED TO SAVE THE SECTION X, Y, Z
LOCATION FOR A411 IN WHICH CALCULATES THE CORRESPONDING
DISPLACEMENT THICKNESS
WHERE X, Y, Z SHOULD BE THE WING SURFACE LOCATION
FOR THE CURRENT RUN

FILE11 IS USED TO READ IN THE DISPLACEMENT
THICKNESS FROM A411 IN

FILE12 IS USED TO REPLACE PART OF THE INPUT CARDS
BY CARD IMAGES

TAPE13 IS USED TO SAVE PART OF THE CUPUT
SKIPPED FROM THE LINE PRINTER

TAPE14 IS USED TO SAVE THE VELCCITY POTENTIAL
FOR FUTURE USE
*****
COMMON
1      G(161,18,3),SO(161,35),VORT(115),ZV(115),
2      IV(161,35),ITE1(35),ITE2(35),
3      AO(161),BO(18),XO(35),YC(35),ZO(35),SCAL(35),
4      IX,AY,NZ,KTE1,KTE2,ISYM,KSYM,FUS,
      YAW,CYAW,SYAW,ALPHA,CA,SA,FMACH,N1,N2,N3,IO
COMMON /CPF/NL
COMMON /PCKR/ PTCK
COMMON /FLC/ P1, P2, P3, FRES, IRES, JRES, KRES,ARES,CG,IG,JG,KG,AG,NSUP
COMMON /PARMT3/ XT3(161), YT3(161), ZT3(161),
      UT3(161), VT3(161), WT3(161), NO1,Z
COMMON /PRS/ XOC(161),
      XS(161,11),YS(161,11),ZS(11),XLE(11),YLE(11),
      SLOFT(11),TRAIL(11),NP(11),EL(11),E2(11),E3(11),
      DI(161),D2(161),D3(161),SN(161),
      SV(161),SM(161),CP(161),XP(161),YP(161),
      YPO(35),ZPO(35),XMAX(35),XMIN(35),YMAX(35),YMIN(35),
      CHORD(35),SCL(35),SCD(35),SCM(35),TITLE(20),
      FIT(3),COVO(3),P1O(3),P2O(3),P3O(3),FSMOD(3),
      RES(20),CCUNT(20),PTMAP(3),
1 DIMENSION
*****

```



```

C** DUMX(161),DUMY(161),DELR(161)
C** ***** WHICH HAVE RECOMMENDED PROGRAM VALUES *****
C** ***** INPUT PARAMETERS *****
C** *****
XSCAL = 0.0
FCCNT = 0.0
BLCP = 0.0
WEIG = 1.0
PTCK = 0.0
C** *****
ND = 161
NE = 161
KPLCT = 0
IPLCT = 1
ISTCP = 2
N1 = 1
N2 = 1
N3 = 2
REKIND 1 = 1
REKIND 2 = 1
REKIND 3 = 1
REKIND 4 = 1
REKIND 10 = 1
REKIND 13 = 1
REKIND 14 = 1
JO = 0
RAD = 57.295779513082
1 WRITE (6,600)
2 WRITE (6,620)
3 FORMAT(10A460 MCDIFIED FROM FLC27 CF ANTONY JAMESON,,
1 COURANT 50,
2 INSTILLER DIMENSIONAL WING ANALYSIS IN TRANSONIC FLOW,
3 OF THREE FINITE VOLUME SCHEME/
4 USING VERSION, PREPARED BY DR. HAI-CHOW CHEN',
• BOEINGARD BOEING INPUT FORMAT FOR WING SECTION DATA IS USED.)
READ (5,530) TITLE
WRITE (6,630) TITLE
READ (5,500) FNX,FNY,FNZ,FMESH,FPLCT
NX = FNX
NY = FNY
NZ = FNZ
MMESH = FMESH
IF (NX.LT.1) GO TO 301
KPLCT = ABS(FPLCT)
READ (5,500)

```



```

DO 12 NM=1, NMESH
C*** INITIALIZE INPUT PARAMETERS WHICH HAVE RECOMMENDED PROGRAM VALUES ***
C**
P2C(NM) = 0.7
P3C(NM) = 1.0
FSMCO(NM) = 0.0
PTMAP(NM) = 0.0

C**
C***
12 READ (5,510) FIT(NM), CCVO(NM), P10(NM)
READ (5,500)
READ (5,510) FMACH, YA, AL, CDO
CALL GECH (ND, NS, NP, XS, YS, ZS, XLE, YLE, SLOPT, TRAIL, XP, YP,
1 FUS, XTEO, CHORDO, ZTIP, SWEEP, CIHED,
2 FIX, PX, PZ, ISYM0, KSYM)

ALPHA = AL/RAD
IF (BLCF.LE.0.) GO TO 44
IF (PTCK.GE.1.) WRITE (6,600)
READ (11) (TITLE(I), I=1,8), FMACH, ALPHA, NS
DO 40 K=1, NS
READ (11) NPCK
NP(K) = NPCK
NPCK1 = NPCK + 1
READ (11) (DUMX(NPCK1-I), DUMZ, DUMY(NPCK1-I), DELR(NPCK1-I),
1 IF (PTCK.LE.0.) GC TC 30
WRITE (6,52) K, NPCK, NPCK1
WRITE (6,54) (DUMX(NPCK1-I), I=1, NPCK)
1 WRITE (6,54) (XS(I,K), YS(I,K), I=1, NPCK)
CONTINUE
CALL BLIN (XS(1,K), YS(1,K), DELR, WEIG, NPCK, NL)
CONTINUE
CONTINUE
IF (PTCK.GE.1.) GO TC 56
IF (PTCK.GE.1.) WRITE (6,600)
WRITE (10) (TITLE(I), I=1,8), FMACH, ALPHA, NS
DO 50 K=1, NS
NPCK = NPCK + 1
NPCK1 = NPCK + 1
DO 48 I=1, NPCK
DUMX(NPCK1-I) = XS(I,K) + XLE(K)
DUMY(NPCK1-I) = YS(I,K) + YLE(K)
CONTINUE
WRITE (10) NPCK
WRITE (10) (DUMX(I), ZS(K), DUMY(I), I=1, NPCK)
IF (PTCK.LE.0.) GO TO 49
48

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```

WRITE (6,52) K,NPCK,K,NPCK1,ZS(K)
WRITE (6,54) (DUMX(I),ZS(K),DUMY(I),I=1,NPCK)
45 CONTINUE
50 CONTINUE 10
52 FORMAT (1H0,5X,3I5,F11.4/)
54 FORMAT (12F11.4)
56 CONTINUE
IF (KSYM.NE.0) YA = 0.
ISYM = ISYMO
IF (AL.NE.0) ISYM = 0
YAW = YA/RAD
CYAW = COS(YAW)
SYAW = SIN(YAW)
CA = CYAW*COS(ALPHA)
SA = CYAW*SIN(ALPHA)
IF (FCCNT.LT.1) GC TC 91
REAC (4) = NX,NY,NZ,NM,K1,K2,NIT
MX = NX +1
MY = NY +2
MZ = NZ +3
DO 62 K=1,MZ
READ (4) ((G(I,J,1),I=1,MX),J=1,MY)
BUFFER (N3,1) (G(1,1,1),G(MX,MY,1))
WRITE (N3) ((G(I,J,1),I=1,MX),J=1,MY)
IF (UNIT(N3).GT.0) GO TO 1
BUFFER (N1,1) (G(1,1,1),G(MX,MY,1))
WRITE (N1) ((G(I,J,1),I=1,MX),J=1,MY)
IF (UNIT(N1).GT.0) GO TO 1
62 CONTINUE (VORT(K),K=K1,K2)
READ (4)
REWIND N3
REWIND N1
REWIND 4
91 CALL CCCRD (NX,NY,NZ,KSYM,ZTIP,XLIM,ZLIM,
SY,AX,AZ,PX,PZ,AC,BC,ZO)
CALL SINGL (NS,NZ,KSYM,KTE1,KTE2,FUS,CHCRD0,ZS,XLE,YLE,
SWEEP,DIHED,XO,YO,ZO,YFO,ZPC,E1,E2,E3,IND)
CALL SUFF (ND,NE,NS,NX,NZ,ISYM,KSYM,KTE1,KTE2,
YAW,XTEO,XLIM,FIX,NP,XS,SLOP,I,TRAIL,
AO,XO,ZO,SO,SCAL,ZV,IV,IIE1,IIE2,
XP,YP,SN,D1,D2,D3,IND)
IF (INC.EC.C) GC TC 291
IF (FCCNT.GE.1) GO TO 101
NM = 1
NIT = 0
CALL ESTIM
IF (IG.EC.0) GO TO 1

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C C C C


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REWIND N2
REWIND N1
101 IF (PTCK .GE. 1.) WRITE (6,600)
    FCNT = 0
    COV = COVG(NM)
    P1 = P10(NM)
    P2 = P20(NM)
    P3 = P30(NM)
    MIT = FIT(NM) + NIT
    KIT = MIT
    IF (KIT.LT.2) KIT=2
    JI = NIT
    LRES = 0
    MRRES = 0
    MX = NX +1
    MY = NY +2
    MZ = NZ +3
    KY = NY +1
    K1 = 1
    K2 = NZ +1
    IF (KSYM.EC.0) GO TC 103
    K1 = 3
    K2 = NZ +3
    LZ = NZ/2 +1
    IF (KSYM.NE.0) LZ = 3
    IF (PTCK.LE. 0.) GC TC 108
    WRITE (6,104)
104 FORMAT(48HINDICATION OF LOCATION OF WING AND VORTEX SHEET,
1
2
27H IN CCGRDINATE PLANE Y = 0./
27H((IV(I,K),K=K1,K2),I=1,MX))
    DO 106 I=1,MX
106 WRITE (6,650) (IV(I,K),K=K1,K2)
108 CONTINUE
    IMAP = FTMAP(NM)
    IF (IMAF.EQ. 0) GC TC 830
    WRITE (6,600)
    WRITE (6,112)
112 FORMAT(49HCHORDWISE CELL DISTRIBUTION IN SQUARE ROOT PLANE, TIP)
    DO 820 ISEC = LZ,KTE2,IMAP
1
812 WRITE (6,812) ISEC,ZP0(ISEC)
    FORMAT(15H0 I X ,20H SECTION PROFILE NO.,
1
2
12,3X,12=,G1E.4)
820 CALL PPFY (2,NX,A0,S0(1,ISEC))
83C CONTINUE
    IF (PTCK.LE. 0.) GC TC 130
    WRITE (6,116)

```



```

116 FORMAT(15F0,15H PCWER LAW )
WRITE(6,610) XLIM,AX
WRITE(6,600)
WRITE(6,118)
118 FORMAT(46H0NORMAL CELL DISTRIBUTION IN SQUARE ROOT PLANE/
15F0,15H
DO 120 J=1,KY
120 WRITE(6,610) BC(J)
122 FORMAT(15F0,15H PCWER LAW )
WRITE(6,610) SY,AY
WRITE(6,600)
WRITE(6,124)
124 FORMAT(45H0SPANWISE CELL DISTRIBUTION AND SINGULAR LINE/
15F0,15H X SING,15H Y SING )
DO 126 K=K1,K2
126 WRITE(6,610) ZO(K),XO(K),VO(K)
128 FORMAT(15H0 TIP LOCATION,15H PCWER LAW )
WRITE(6,610) ZLIM,AZ
130 CONTINUE
WRITE(6,600)
WRITE(6,132)
132 FORMAT(15H0ITERATIVE SOLUTION)
134 WRITE(6,134) MACH NO,15H YAW,15H ANG OF ATTACK)
FORMAT(15H0 FMACH,YA,AL,15H NZ )
WRITE(6,610) NX,NY,NZ,15H
136 FORMAT(15H0 RELAX FCT 1,15H RELAX FCT 2,15H RELAX FCT 3 )
WRITE(6,610) P10(NM),P20(NM),P30(NM)
140 FORMAT(10H0ITERATION,15H MAX CORREC,4H I,4F J,4H K,15H AVG CORREC,
15H MAX RESIDUAL,4H I,4F J,4H K,15H AVG RESIDAL,
12H CIRCULATION,15H SONIC PIS)
141 NIT = NIT + 1
JIT = JIT + 1
CALL MIXFLC
IF (10.EC-0) GO TO 151
142 N1 = N1
143 N2 = N2
144 N3 = N3

```



```

N3      = N
WRITE (6,66C) NIT,DG,IG,JG,KG,AG,FRES,IFES,JRES,KRES,ARES,
1      VGR1(LZ),NSUP
      LRES = LRES
      IF (LRES.EQ.MRES) LRES = 1
      IF (LRES.NE.1) GO TO 143
      NRES = NRES
      COUNT(NRES) = NRES
      RES(NRES) = FRES
      IF (JIT.GE.KIT) GO TO 251
      IF (NM.LE.1) .OR. NM.LT.MMESH) GO TO 148
      IF (ABS(DG).LE.COV) GO TC 251
148     CONTINUE
      IF (NIT.LT.MIT .AND. ABS(DG).GT.COV .AND. ABS(DG).LT.10.) GO TO 141
      GO TO 161
151     IF (JO.EQ.1) GO TO 1
      REWIND A1
      REWIND A2
      JO
      N
      N3
      N2
      N1
      N
      GO TO 141
161     RATE = 0.
      IF (NRES.GT.1) RATE = (ABS(RES(NRES)/RES(1))) - COUNT(1)))
1      WRITE (6,162) MAX RESIDUAL 1,15H MAX RESIDUAL 2,15H
162     FORMAT(15H0 MAX RESIDUAL 1,15H MAX RESIDUAL 2,15H
1      15H REDUCTN/CYCLE, 15H CONV TOLERANCE)
      WRITE (6,670) RES(1),RES(NRES),COUNT(NRES),RATE
1.CCV
      WRITE (6,600)
      DO 164 N=1,3
      BUFFER IN (N1,1) (G(1,1,M),G(MX,MY,M))
      REAC (N1,ERR=151) ((G(1,J,M),I=1,MX),J=1,MY)
      IF (UNIT(N1).GT.0.) GO TO 151
164     CONTINUE
      LX = NX/2 + 1
      K
      KKK
      KKK
      IF (NM.LT.MMESH) GO TO 17C
      REWIND 8
      REWIND 8
      NRC = KIE2 - KIE1 + 1
      WRITE (6) (TITLE(I),I=1,8),FMACH,ALPHA,NRC
17C     CONTINUE

```

WORK ,


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171 K IF (K.EC.MZ) GO TO 191
DO 172 J=1,MX
DO 172 I=1,MX
G(I,J,1) = G(I,J,2)
G(I,J,2) = G(I,J,3)
BUFFER IN (N1,I) (G(I,1,3),G(MX,MY,3))
READ (N1,ERR=151) ((G(I,J,3),I=1,MX),J=1,MY)
C
C IF (UNIT(N1).GT.0.) GO TO 151
IF (K.LI.KTEL.OR.K.GT.KTE2) GO TO 171
CALL VELO (K,SV,SM,CP,XP,YP,XMAX(K),XMIN(K),YMAX(K),YMIN(K))
I1 = ITEL(K)
I2 = ITE2(K)
CHCRD(K) = XP(I1) -XP(LX)
CALL FCRCF (I1,I2,XP,YP,CP,AL,CHORD(K),XO(K),YPO(K),
1 SCL(K),SCD(K),SCM(K))
KKK = KKK +1
IF (KPLCT.GT.1.AND.K.GT.KTEL) GC TC 185
IF (KPLCT.EQ.0.AND.KKK.GT.1) GO TO 185
WRITE (6,600)
WRITE (6,182)
182 FORMAT(24HSECTION CHARACTERISTICS/
15H0 MACH NO ,15H YAW
15H FMACH,YA,AL
184 WRITE (6,610)
WRITE (6,184)
184 FORMAT(15HOSPAN STATION ,15H CL
15H CM
185 WRITE (6,610) ZPO(K),SCL(K),SCD(K),SCM(K)
Z = ZPC(K)
IF (MIT.LE.0) GC TO 850
IF (KPLCT.LE.2) CALL CPLOT (2,NX,FMACH,XP,YF,CP,SM,I1,I2,KPLOT)
850 CONTINUE
WRITE CNE FILE ON TAPE 8
IF (NM.LI.NMESH) GO TO 186
WRITE (8) NCI
WRITE (8) (XT3(I),ZT3(I),YT3(I),UT3(I),VT3(I),I=1,NOI)
NR C=12-11+1
C
WRITE CP VS X/C SECTION DATA FOR FINAL MESH ON TAPE 9
WRITE (5,900) ZPO(K)
WRITE (5,910) NRD
WRITE (5,920)
WRITE (5,950) (XQCD(J),CP(J),J=1,12)
FORMAT (/,14HSPAN STATION =,F12.5)
900 FORMAT (1X,20HNC. CF DATA POINTS =,I5)
910 FORMAT (1X,6H X/C,8X,2HCP,7X,3HX/C,8X,2HCF,7X,3HX/C,8X,2HCP,
920 17X,3HX/C,8X,2HCF,3X)
950 FORMAT (8F10.6)
186 CONTINUE

```



```

C WHEN KPLOT = 2 CALL SUBROUTINE VERTEC WHICH PLOTS CP VS X/C
C FOR EACH SECTION OF THE FINAL MESH
C
1 IF (KPLOT.EC.2.AND.NM.EQ.MMESH) CALL VERTEC(I1,I2,XOCD,CP,NRD,
1 ZPO,FMACH,YA,AL,SCL,SCD,SCM,K)
GO TO 171
191 CONTINUE
IF(NM.LT.MMESH)GO TC 200
ENCFIL 8
REWIND 8
ENDFIL 5
REWIND 5
CONTINUE
200 CALL TCTFOR (KTE1,KTE2,CHORD,SCL,SCD,SCM,XC,YPO,ZPO,
1 CL,CD1,CMP,CMR,CMY,
1 CD1 = CYAW*CD1
CD = CDO +CD1
VLC1 = 0
IF (ABS(CD1).GT.1.E-6) VLD1 = CL/CD1
VLC = 0
IF (ABS(CD).GT.1.E-6) VLD = CL/CD
WRITE (6,60C)
WRITE (6,192)
192 FORMAT(21HLOWING CHARACTERISTICS/
1 MACH NO ,15H YAW
1 FMACH,YA,AL
1 WRITE (6,610)
WRITE (6,154)
194 FORMAT(15H
1 CL ,15H CD FORM
1 CD ,15H L/C FORM
1 CL,CD1,CDO,CD,VLD1,VLC
1 CM YAW ,15H CM RCLL
196 WRITE (6,610) CMY,CMR,CMP
REWIND 11
IF (KPLOT.LT.1) GO TO 201
CALL RPLOT (IPLCT,NRES,RES,COUNT,TITLE,FMACH,YA,AL,NX,NY,NZ)
CALL DRAW (IPLCT,XMAX,XMIN,YMAX,YMIN,ZPO,FUS,TITLE,NZ,KTE1,KTE2)
CALL T-FREED (IPLCT,SV,SM,CP,XP,YP,ZPO,TITLE,YA,AL,
1 VLD,CL,CD,CHORDO,XSCAL,PSCAL)
1 IF (IO.EQ.0) GO TO 151
IF (ISICP.EQ.1) GO TO 301
201 IF (NM.LT.MMESH) GC TC 203
GO TO 1
203 CONTINUE
NX = NX +NX
NY = NY +NY
NZ = NZ +NZ

```



```

CALL CCCRD (NX,NY,NZ,KSYM,ZTIP,XLIM,ZLIM,
1 SY,AX,AZ,PX,PZ,AO,BC,ZO)
1 CALL SINGL (NS,NZ,KSYM,KTE1,KTE2,FUS,CHCRDO,ZS,XLE,YLE,
1 SWEEP,DIHED,XO,YO,ZO,YPC,ZPC,E1,E2,E3,IND)
1 CALL SUFF (ND,NE,NS,NX,NZ,ISYM,KSYM,KTE1,KTE2,
1 YAW,XTEQ,XLIM,FIX,NP,XS,YE1,ITE1,ITE2,
2 AO,XO,ZO,SO,SCAL,ZV,IV,ITE1,ITE2,
3 XP,YP,SN,C1,D2,D3,IND)
IF (INC.EQ.0) GC IC 291
CALL REFIN
IF (IO.EQ.0) GO TO 221
REWIND N1
REWIND N2
NSMOO = FSMCC(NM)
IF (NSMCC.LT.1) GO TO 211
DO 202 N=1,NSMCC
CALL SMCC
IF (IO.EQ.0) GO TO 221
REWIND N1
REWIND N2
202 N1 = N1
211 N1 = N2
N2 = N3
N3 = N
NM = NM +1
NIT = 0
GO TO 101
221 NX = NX/2
NY = NY/2
NZ = NZ/2
CALL CCCRD (NX,NY,NZ,KSYM,ZTIP,XLIM,ZLIM,
1 SY,AX,AZ,PX,PZ,AO,BC,ZO)
1 CALL SINGL (NS,NZ,KSYM,KTE1,KTE2,FUS,CHCRDO,ZS,XLE,YLE,
1 SWEEP,DIHED,XO,YO,ZO,YPC,ZPC,E1,E2,E3,IND)
1 CALL SUFF (ND,NE,NS,NX,NZ,ISYM,KSYM,KTE1,KTE2,
1 YAW,XTEQ,XLIM,FIX,NP,XS,YE1,ITE1,ITE2,
2 AO,XO,ZO,SO,SCAL,ZV,IV,ITE1,ITE2,
3 XP,YP,SN,C1,D2,D3,IND)
IF (INC.EQ.0) GC IC 291
GO TO 151
251 K1 = KTE1 -1
K2 = KTE2 +ITE2(KTE2) -NX/2
WRITE (14) NX,NY,NZ,NM,K1,K2,NIT
DO 262 K=1,NZ
BUFFER IN ERR=281) ((G(I,J,I),I=1,MX),J=1,MY)
READ (N1,ERR=281) ((G(I,J,I),I=1,MX),J=1,MY)
IF (UNIT(N1).GT.0) GO TO 281
262 WRITE (14) ((G(I,J,I),I=1,MX),J=1,MY)

```



```

C
REWIND A1
WRITE (14) (VORT(K),K=K1,K2)
ENDFILE 14
REWIND 14
CALL SWITCH(1,ISTOP)
CALL SLIET(1,ISTOP)
IF (ISTCP.EC.1) GO TO 161
J1 7
IF (NIT.LT.MIT.AND.ABS(DG).GT.COV.AND.ABS(DG).LT.10.) GC TO 141
GO TO 161
REWIND 4
281 GO TO 151
291 WRITE (6,600)
292 FORMAT(24HOBAD DATA,SPLINE FAILURE)
301 GO TO 1
CONTINUE
REWIND 10
IF (KPLCT.GT.0) CALL PLOT(0.,0.,955)
STCP
FORMAT(1X)
50C FORMAT(8F10.6)
51C FORMAT(2CA4)
53C
60C FORMAT(1H1) 5,7G15.5)
61C FORMAT(F12.20A4)
63C FORMAT(1H0,7I15)
64C FORMAT(1X,3I13)
65C FORMAT(1I10,E15.5,3I4,E15.5,F10.5,I10,F10.3)
660
67C FORMAT(2E15.4,2F15.4,E15.4)
END

```



```

IF (I.LT.NL) SI = -1.
GO TO 850
820 CONTINUE
S = 0.
DL = DELR(I)
DX = 0.
DY = DL*SI
GO TO 880
850 CONTINUE + DYXN**2
S = 1.
S = SQR1(S)
S = 1./S
F = 1.
IF (DYXN *SI.LT.0.) F = -1.
DL = DELR(I)
DX = S*F
DY = ABS(DYXN)*S*SI
DX = DX * DL
DY = DY * DL
XT(I) = X2 + DX*WEIG
YT(I) = Y2 + DY*WEIG
CONTINUE
880 IF (PTCK .LE. 1.) GO TO 890
WRITE (6,1000) I,F,S,DL,DX,DY,CYXN,XT(I),YT(I),DYX,WEIG
890 CONTINUE
IF (I.EC.N) GO TO 900
X1 = X2
Y1 = Y2
X2 = X3
Y2 = Y3
I = I+1
GO TO 200
900 CONTINUE
RETURN
1000 FORMAT (1H ,I5,F7.2,9G13.5)
END

```



```

C**SUBROUTINE PPXY*****
C  SUBROUTINE PPXY (I1,I2,X,Y)
C  SUBPROGRAM FOR LINE PRINTER PLOTTING OF THE UNWRAPPED
C  WING SECTIONS
COMMON /PCKR/ PTCK
COMMON /SHARE/ LINE(100)
DIMENS ICN X(1),Y(1)
DATA IB /1H /, IP /1H+/, KMAX /100/, ACC /1.5/,
1 IZ /1F/, ICONST /0/
DO 10 I=1,100
LINE(I) = IB
10 CONTINUE
YMAX = -1.0E35
YMIN = -YMAX
WICTH = KMAX - 5
DO 20 I = 11,12
YMAX = AMAX1(YMAX,Y(I))
YMIN = AMIN1(YMIN,Y(I))
20 CONTINUE
VAL = ABS(YMAX) + ABS(YMIN)
S = WICTH/VAL
KK = 0
IF (ICONST.LE.YMAX .AND. ICONST.GE.YMIN) KK = S*(YMAX-ICONST)+ADD
IF (KK.NE.0) LINE(KK)=IZ
DO 30 I=11,12
K = S*(YMAX-Y(I)) + ADD
IF (K.L1.1) K = 1
IF (K.G1.KMAX) K = KMAX
LINE(K) = IP
WRITE (6,100) I,X(I),Y(I),LINE
LINE(K) = IB
IF (K.EC.KK) LINE(KK) = IZ
30 CONTINUE
RETURN
100 FORMAT (1X,I3,2F10.4,4X,100A1)
ENC

```



```

C**SUBROUTINE LSQR*****
SUBROUTINE LSQR (NL,NB,XP,YP,XSING,YSING)
SUBPROGRAM FOR WING SECTION LEADING EDGE SINGULAR POINT
CALCULATION BY MEANS OF COMPUTING THE FCCUS OF A
PARABOLA BY NB*2+1 POINTS LEAST-SQUARE FIT CENTERED AT
THE LEADING EDGE
NB: SUPPLY BY THE CALLING PROGRAM GEOM
COMMON /FCKR/ FTCK
DIMENSION XP(1),YP(1)
N1 = NL - NB
N2 = NL + NB
N = N2 - N1 + 1
A1 = N
B1 = 0.
C1 = 0.
A2 = 0.
B2 = 0.
C2 = 0.
A3 = 0.
B3 = 0.
C3 = 0.
D1 = 0.
D2 = 0.
D3 = 0.
SCALE2 = 100.
SCALE2 = 500.
DO 300 I = N1,N2
  YY = (YP(I) - YP(NL))*SCALE
  B1 = B1 + YY
  C1 = C1 + YP2
  YP3 = C2 + YP3
  YP4 = C3 + YP4
  C3 = XP(I)*SCALE2
  XX = D1 + XX
  YX = Y1 + YX
  D2 = D2 + YF2
  Y2X = D3 + Y2X
300 D3 = D3 + B1
  A2 = C1
  B2 = C2
  A3 = C3
  B3 = C3

```



```

DXAM = CXA
DXAM = CXA
DX2M = DXAM**2
60C CONTINUE
IF (PTCK .LE. 0.) GC TC 65C
WRITE (6,70C) I,X,Y,DX,DX2,R2,CXAM,DX2M,XP(1),YP(1)
65C CONTINUE
IF (PTCK .LE. 0.) GC TC 75C
RA = R2/A1
WRITE (6,70C) N,RA,DXAM
70C FORMAT (113,9G13.5)
75C CONTINUE
RETURN
ENTRY LSC
IF (DXAM.LE.1.E-4) RETURN
WRITE (6,80C) DXAM
80C FORMAT (1H0,5X,'WARNING ??? DEVIATION GF THE LEADING EDGE PCINIS',
1, FROM PARABOLA IS GREATER THAN 0.0001',6X,'DXAM =',G13.4//)
RETURN
END

```



```

ISYMO      = 1
XTEC       = 0.
CHORDO     = 0.
K          = 1
11 READ    (5,500) ZS(K),XL,YL,CHORD,THICK,AL,FSEC
READ       (5,510) ZS1 = ZS(1)
IF (K.EC.1) ZS1 = AL/RAD
ALPHA      = AL/RAD
IF (K.GT.1.AND.FSEC.EQ.0.) GO TO 31
READ       (5,500)
READ       (5,510) FN
N          = FN
READ       (5,500)
N1 = N + 1
READ       (5,520) (XP(N1-1),YP(N1-1),I=1,N)
FORMAT     (6F10.0)
52C DO 26 I=1,N
IF (XP(I+1).LT.XP(I)) GC TC 26
NL = I
GO TO 800
26 CONTINUE
800 IF (FNE.LE.0.) GC TO 21
DYL = YF(1) - YF(2)
DXL = XF(1) - XF(2)
DYU = YF(N) - YF(N-1)
DXU = XF(N) - XF(N-1)
TSU = CYU/DXU
TSL = CYL/DXL
TRL = ATAN2(DYL,DXL) - ATAN2(DYU,DXU)
TRL = TRL*RAD
SLT = (TSL+TSU)*.5
NB = FNE
CALL LSCR (NL,NE,XP,YP,XSING,YSING)
21 WRITE   (6,600) ZS(K)
22 WRITE   (6,600) FILE AT Z = ,F10.5/ TE SLCP E ,15H X SING ,
FORMAT     (16F10.0)
15H0
15H
21 WRITE   (6,610) TRL,SLT,XSING,YSING
27 WRITE   (6,620) NL,XP(NL),XP(1),YP(1),I=1,N)
62C FORMAT (////,NL=,I3,,XP(NL) = ,F10.5 // (XP,YP)'//
1
2
31 SCALE = CHORD/(XP(1) -XP(NL))
XLE(K) = XL + (XSING -XP(NL))*THICK*SCALE
YLE(K) = YL + (YSING -YP(NL))*THICK*SCALE
XX      = XP(NL) + (XSING -XP(NL))*THICK
YY      = YP(NL) + (YSING -YP(NL))*THICK

```



```

CA      = COS(ALPHA)
SA      = SIN(ALPHA)
DO 22 I=1,N
  XS(I,K) = SCALE*((XP(I) -XX)*CA +THICK*(YP(I) -YY)*SA)
  YS(I,K) = SCALE*(THICK*(YP(I) -YY)*CA - (XP(I) -XX)*SA)
32 SLOPT(K) = THICK*SLT -TAN(ALPHA)
  TRAIL(K) = THICK*TRL/RAD
  NP(K) = N
  CHORDO = AMAX1(CHORDO,CHORD)
  IF (YS*LE.O. CR.ALPHA*NE.O.) ISYMC = C
  WRITE (6,42) ZS(K)
42 FORMAT (27F10.5)
1 15H0 XLE RATIO,15H YLE TWIST ,15H
  WRITE (6,610) XL,YL,CHORD,THICK,AL
  YMIN = YP(NL)
  YMAX = YP(NL)
DO 44 I = 1,N
  IF (YP(I) .GE. YMIN) GC TO 43
  JMIN = I
  YMIN = YP(I)
43 IF (YP(I) .LE. YMAX) GC TO 44
  JMAX = I
  YMAX = YP(I)
44 CONTINUE
  YDIF = YMAX - YMIN
  NN = N - 1
  SUM = C.
DO 46 I = NL,NN
  SUM = SUM + .5*(YP(I)+YP(I+1))*(XP(I+1)-XP(I))
46 CONTINUE
  NM = NL - 1
DO 48 I = 1,NM
  SUM = SUM + .5*(YP(I)+YP(I+1))*(XP(I+1)-XP(I))
48 CONTINUE
30C WRITE (6,300)
  15H0 JMAX YMIN ,15H YDIF JMIN ,15H AREA
320 FORMAT (15H ,G12.4,111,G19.4,111,G19.4,G15.4)
  WRITE (6,320) YMIN,JMIN,YMAX,JMAX,YDIF,SUM
  CALL LSC
  IF (FUS*LE.O.) GO TO 61
  R = AMAX1(0.,(FUS**2 - YLE(1)**2))
  Z = ZS(K) - ZS1 + SQRTR(R)
  R = FUS**2/(YLE(K)**2 +Z**2)
  ZS(K) = Z*(1. -R)
  YLE(K) = YLE(K)*(1. +R)
  S = R*XS(NL,K)

```



```

XLE(K) = XLE(K) -S
DO 52 I=1,N XS(I,K) +S
XS(I,K) = YS(I,K)* (1. +R)
52 K = K +1
61 IF (K.LE.NS) GO TO 11
Z0 = ZS(1) +ZS(NS)
IF (KSYM.NE.0) Z0 = ZS(1)
DO 62 K=1,NS
XTEO = AMAX1(XTEO,XS(1,K))
62 ZS(K) = ZS(K) -Z0
ZTIP = ZS(NS)
RETURN
500 FORMAT(1X)
510 FORMAT(8F10.6)
60C FORMAT(1H1)
61C FORMAT(F12.4,7F15.4)
ENC

```



```

C**SUBROUTINE COORD*****
SUPERROUTINE COORD (NX,NY,NZ,KSVM,ZIIP,XLIM,ZLIM,
1 SETS UP STRETCHED PARABOLIC AND SPANWISE COORDINATES
DIMENSION AO(1),BO(1),ZO(1)
PI BOUND = 3.1415926535898
AX = .95
AY = .5
AZ = .5
XLIM = .625*BCUND
ZLIM = .625*BCUND
SY SCALZ = ZIIP/(1.000001*ZLIM)
LX = NX/2 +1
NX = 2.*BCUND/NX
DX = PI/XLIM
Q = PX/C
R = 1./(1. +R*SIN(Q) -XLIM)
DO 12 I=1,MX
C (I -LX)*DX
D = D +R*SIN(C*D)
IF (ABS(D).LE.XLIM) GO TO 12
B IF (D.LT.0.) B = -1.
A = 1. - (C -B*XLIM)*E)**2
C = A**AX
D = B*XLIM +(D -B*XLIM)/C
12 AO(I) = D
DY = NY +1
DO 22 J=1,KY
D = (KY -J)*DY
A = 1. -D*D
C = A**AY
22 BO(J) = SY*D/C
LZ = NZ/2 +1
K1 = 1
K2 = NZ +1
DZ = 2.*BCUND/NZ
Q = PI/ZLIM
R = PZ/C
IF (KSVM.EQ.0) GO TO 31
LZ = 3
K1 = 2
K2 = NZ +3
DZ = BOUND/NZ

```



```

      Q = Q + Q
      R = -PZ/Q
      31 DO 32 K=K1,K2      +R*SIN(Q)  -ZLIM)
      D = 1./(1.          -LZ)*DZ
      D = (K  +R*SIN(Q*D)
      IF (ABS(C).LE.ZLIM) GC TO 32
      B = 1.
      IF (D.LT.0.) B = -1.
      A = 1.          -(C  -B*ZLIM)*E)**2
      C = A**AZ
      D = B*ZLIM  +(D  -B*ZLIM)/C
      D = SCALZ*C
      32 ZO(K)
      RETURN
      END

```



```

C**SUBROUTINE SINGL (NS,NZ,KSYM,KTE1,KTE2,FUS,CHORDO,ZS,XLE,YLE,
SUBROUTINE SINGL (NS,NZ,KSYM,KTE1,KTE2,FUS,CHORDO,ZS,XLE,YLE,
1 GENERATES SINGULAR LINE FOR SQUARE ROOT TRANSFORMATION
DIMENSION ZS(1),XLE(1),YLE(1),XO(1),YC(1),ZO(1),YPO(1),ZPO(1),
1 K1
K2 = NZ +1
IF (KSYM.EC.O) GO TC 11
K1 = 2
K2 = NZ +3
KTE1 = 3
11 DO 12 K=K1,K2
IF (ZC(K).LT.ZS(1)) KTE1 = K +1
IF (ZC(K).LE.ZS(NS)) KTE2 = K
12 CONTINUE
CALL SFLIF (1,NS,ZS,XLE,E1,E2,E3,2,0,2,0,0,0,IND)
CALL INTPL (KTE1,KTE2,ZO,XO,1,NS,ZS,XLE,E1,E2,E3,0)
S1 = CHORDO*E1(1)
S2 = CHORDO*E1(NS)
CALL SFLIF (1,NS,ZS,YLE,E1,E2,E3,2,0,2,0,0,IND)
CALL INTPL (KTE1,KTE2,ZO,YO,1,NS,ZS,YLE,E1,E2,E3,0)
T1 = CHORDO*E1(1)
T2 = CHORDO*E1(NS)
XO(KTE1-1) = XO(KTE1) -XO(KTE1+1)
YO(KTE1-1) = YO(KTE1) -YO(KTE1+1)
IF (KSYM.NE.O) GO TO 31
N = KTE1 -1
DO 22 K=K1,N
ZZ = (ZO(K) -ZO(KTE1))/CHORDO
A = EXP(ZZ)
XO(K) = XO(KTE1) +S*ZZ -(S1 -T1)*(1. -A)
YO(K) = YO(KTE1) +T*ZZ -(T1 -T2)*(1. -A)
22 N
31 N = K=N,K2
DO 32 K=N,K2
ZZ = (ZO(K) -ZO(KTE2))/CHORDO
A = EXP(-ZZ)
XO(K) = XO(KTE2) +S*ZZ +(S2 -T2)*(1. -A)
YO(K) = YO(KTE2) +T*ZZ +(T2 -T1)*(1. -A)
32 YO(K)
DO 42 K=K1,K2
YPO(K) = YO(K)
ZPO(K) = ZO(K)
IF (FUS.LE.C.) GO TC 42
A = .25*(ZO(K)**2 -YO(K)**2) +FUS**2
B = .5*ZO(K)*YO(K)
S = SQR(A**2 +B**2)

```



```

T      = 0.
IF (S.GT.0.) T = .5*ATAN2(B,A)
S      = SQR(T(S))
YP0(K) = .5*Y0(K) + S*SIN(T)
ZP0(K) = .5*Z0(K) + S*COS(T)
42 CONTINUE
      RETURN
      ENC

```



```

C**SUBROUTINE SURF*****
SUBROUTINE SURF (ND,NE,NS,NX,NZ,ISYM,KSYM,KTE1,KTE2,
1 YAW,XTEO,XLIM,FX,NP,XS,ZS,SLOPT,TRAIL,
2 AO,XO,ZO,SO,SCAL,ZV,IV,ITE1,ITE2,
3 XP,YP,SN,DI,L2,L3,INL)
C INTERPLATES MAPPED WING SURFACE AT MESH POINTS
DIMENSION SO(NE,1),XS(ND,1),YS(ND,1),ZS(1),SLOPT(1),TRAIL(1),
1 AO(1),XO(1),ZO(1),SCAL(1),ZV(1),
2 XP(1),YP(1),SN(1),DI(1),D2(1),D3(1),
3 IV(NE,1),NP(1),ITE1(1),ITE2(1),
PI=3.141592653589E
TVAW=TAN(YAW)
SSO=XTEO/XLIM**2
DX=2./NX +1
LX=NX +1
MX=NX +3
MZ=NX +3
IV0=1 -ISYM -ISYM -ISYM
IV1=1 -ISYM -ISYM
DO 2 K=1,MZ
ITE1(K)=MX
ITE2(K)=MX
DO 2 I=1,NX
IV(I,K)=-2
SO(I,K)=0.KTE1
2 K K2 K1 R2
21 K2 K1 R2
23 R1 R2
25 R2 I2
IF (ZS(K2)) 21,25,23
IF (Z0(K)) -ZS(K1)/(ZS(K2) -ZS(K1))
R1=-R2
I2=(I3*NX)/16 +1
IF (FIX.EQ.C.) GO TO 31
IF (FIX.EQ.C.) +R2*XS(1,K2)
C CC=SQRT(C/SSO)
DO 26 I=2,NX
IF ((AC(1)) +.5*DX).LT.-CC) I1=I +1
IF ((AC(1)) -.5*DX).LT.CC) I2=I
CON=INLE
26 KK RR
31 KK RR
41 N ANGL
U V
= K1
= R1(KK)
= NP(KK) +PI
= 1.
= 0.

```



```

DO 42 I=1,N
R = SQRT(XS(I,KK)**2 +YS(I,KK)**2)
IF (R.EC.C.) GO TO 43
ANGL = ANGL +ATAN2((U*YS(I,KK) -V*XS(I,KK)),
1 U (U*XS(I,KK) +V*YS(I,KK)))
V = XS(I,KK)
= YS(I,KK)
R = SQRT(R**2 +R)
R*CCS(.5*ANGL)
GO TO 42
43 ANGL = PI
U = -1.
V = 0.
XP(I) = 0.
YP(I) = 0.
42 CONTINUE
SS = AO(I2)/AMIN1(ABS(XP(1)),ABS(XP(N)))
DO 44 I=1,N
XP(I) = S*XF(I)
YP(I) = S*YF(I)
ANGL1 = ATAN(SLOPT(KK))
ANGL2 = ATAN(YS(1,KK)/XS(1,KK))
ANGL1 = ATAN(YS(N,KK)/XS(N,KK))
ANGL2 = ATAN(-.5*(ANGL1 -TRAIL(KK)))
T1 = ANGL -.5*(ANGL2 +TRAIL(KK))
T2 = TAN(ANGL1)
CALL SPLIF (1,N,XP,YP,D1,D2,D3,1,T1,1,T2,0,0,IND)
IF (INC.EC.O) WRITE (6,500) KK,K1,K2,N,RR,R1,R2,ZS(KK)
500 FORMAT (12HOBAC MAPPING,4I10,4G13.4/)
CALL INTPL (I1,I2,A0,SA,1,A,XP,YP,C1,D2,D3,C)
X1 = .25*XS(I,KK)
A = SLOPT(KK)*(XS(1,KK) -X1)
B = 1./(XS(1,KK) -X1)
ANGL = PI +PI
U = 1.
V = 0.
M = I1 -1
DO 52 I=2,M
XX = SS*A0(I)**2
YY = B*(XX -X1)
R = YS(1,KK) +A*ALOG(D)/D
ANGL = SQRT(XX**2 +YY**2)
U = ANGL +ATAN2((U*YY -V*XX),(U*XX +V*YY))
V = XX

```



```

52 SN(I) = S*SCRT(R +R)
A = R*SIN(.5*ANGL)
B = SLGFT(KK)*(XS(N,KK) -X1)
U = 1./(XS(N,KK) -X1)
V = 0.
M = 0.
DO 54 I=M,NX
XX = I2 +1
D = SS*AO(I)**2
YY = B*(XX -X1)
R = YS(N,KK) +A*ALOG(D)/D
ANGL = SQRT(XX**2 +YY**2)
U = ANGL +ATAN2((U*YY -V*XX),(U*XX +V*YY))
V = XX
R = YY
54 SN(I) = S*SCRT(R +R)
DO 62 I=2,NX
62 SO(I,K) = SO(I,K) +RR*SN(I)
KK = KK +K2
RR = R2
GO TO 41
71 SS = SS0
IF (FIX.EQ.0.) = (R1*XS(1,K1) +R2*XS(1,K2))/(A0(I1)**2 -S0(I1,K)**2)
1SS = SS +S5
SCAL(K) = SS
ITE1(K) = I1
ITE2(K) = I2
ZV(K) = ZO(K) -TYAW*(XO(K) +SS*AC(I1)*A0(I1))
DO 72 I=I1,I2
72 IV(I,K) = I2
M = I1 -1
DO 74 I=1,M
ZZ = ZO(K) -TYAW*(XO(K) +SS*AO(I)*A0(I))
IF (ZZ.GE.ZV(KTEL)) IV(I,K) = IVO
74 CONTINUE
M = I2 +1
DO 76 I=M,MX
ZZ = ZO(K) -TYAW*(XO(K) +SS*AO(I)*A0(I))
IF (ZZ.GE.ZV(KTEL)) IV(I,K) = IVO
76 CONTINUE
K2 = K2 -1
K = K +1
IF (K.LE.KTEL2) GO TO 21
K1 = K2
K2 = NZ

```



```

IF (KSYM.EQ.0) GC TC 81
K1 = 3
K2 = NZ +2
81 SCAL(K) = SCAL(KTE2)
DO 82 I=1,MX
ZZ = ZO(K) -TYAW*(XO(K) +SS*A0(I)*A0(I))
IF (ZZ.LE.ZS(NS).AND.ZZ.GE.ZV(KTE1)) IV(I,K) = IVO
82 CONTINUE
K = K +1
IF (K.LE.K2) GO TO 81
SCAL(K) = SCAL(KTE2)
N = KTE2
IF (YAW.LE.0.) GO TC 93
IO = ITE1(KTE2) +1
DO 92 I=10,LX
N = N +1
ZV(N) = ZO(KTE2) -TYAW*(XO(KTE2) +SS*A0(I)*A0(I))
92 I = ITE1(KTE1)
93 ZV(KTE1-1) = ZO(KTE1-1) -TYAW*(XC(KTE1) +SS*A0(I)*A0(I))
ZV(N+1) = ZO(KTE2+1)
DO 102 K=K1,K2
DO 104 I=2,NX
IF (IV(I,K).GT.0) GC TC 104
IF (IV(I+1,K+1).GT.C.OR.IV(I-1,K+1).GT.C) IV(I,K) = IV1
IF (IV(I+1,K-1).GT.0.OR.IV(I-1,K-1).GT.C) IV(I,K) = IV1
104 CONTINUE
102 IF (SO(LX,K).LT.1.E-05) IV(LX,K) = 0
IF (KSYM.NE.0) RETURN
N = KTE1 -1
DO 112 K=1,N
SCAL(K) = SCAL(KTE1)
112 RETURN
END

```



```

C**SUBROUTINE ESTIM*****
C  SUPEROUTINE ESTIM*****
C
C  INITIAL ESTIMATE OF REDUCED POTENTIAL
COMMON
1  IV(161,18,3),SO(161,35),VORI(115),ZV(115),
2  IV(161,35),ITE1(35),ITE2(35),
3  AO(161,18),BO(18),XO(35),YC(35),ZC(35),SCAL(35),
4  NX,NY,NZ,KTE1,KTE2,ISYM,KSYM,FUS,
   YAW,CYAW,SYAW,ALPHA,CA,SA,FACH,N1,N2,N3,IC
   = NX +1
   = NY +2
   = NZ +3
DO 12 I=1,161
DO 12 J=1,18
DO 12 K=1,3
12  G(I,J,K)=0.
DO 22 I=1,MZ
DO 22 J=1,18
DO 22 K=1,3
22  WRITE(N3)((G(I,J,1),I=1,MX),J=1,MX)
22  WRITE(N1)((G(I,J,1),I=1,MX),J=1,MX)
22  CONTINUE
K1 = KTE1 -1
K2 = KTE2 +ITE2(KTE2) -NX/2
DO 32 K=K1,K2
32  VORT(K)=0.
DO 10 I=1
10  RETURN
END

```



```

C**SUBROUTINE MIXFLO*****
SUBROUTINE MIXFLO*****
SOLUTION OF EQUATION SCHEME FOR MIXED SUBSONIC AND SUPERSONIC FLOW
USING FINITE VOLUME SCHEME
COMMON
1 2 3 4
COMMON/SPA/
1 2 3
COMMON/FLC/
COMMON/SLP/
LX = NX/2 +1
KY = NX +1
MY = NY +2
J1 = 2
IF (FMACH.GE.1.) J1 = 3
TYAW = SYAW/CYAW
FMACH2 = FMACH*2
AAO = 1./FMACH*2 +.2
CL = 2./F1
Q2T = 1./P2 -1.
FRES = 0.
ARES = 0.
DG = 0.
AG = 0.
NSUP = 0
K1 = 3
K2 = NZ +2
IF (KSYM.EQ.1) GO TO 1
IF (FMACH.GE.1.) K1 = 3
K2 = NZ
1 DO 2 M=2,3
2 READ (N1,ERR=101) ((G(I,J,M),I=1,MX),J=1,MY)
CONTINUE
K = 1
NV = KTE1 -1
RV = 2.
DO 12 I=1,MY
DO 12 J=1,MX
G(I,J,1) = G(I,J,2)
GL(I,J) = G(I,J,2)

```


RETURN
END


```

C**SUBROUTINE YSWEEP*****
C  SUPROUTINE YSWEEP
C  ROW RELAXATION
C  FINITE VOLUME
COMMON
1 2 3 4 5
COMMON/SPA/
1 2 3
COMMON/FLG/
COMMON/SWP/
DIMENSION
1 2 3 4 5
DIMENSION
1 2 3
PI
BV
CV
D(1)
E(1)
I2
J
XS
YS
ZS
XS
YS
ZS
S2
S1
SR1
SR2
FS
DO 12 I=1,MX
QA(I)
P(I)
Q(I)

```



```

R(I)      O.
QP(I)     O.
FU(I)     O.
FW(I)     O.
CG(I)     O.
XM(I)     O.
YM(I)     O.
ZM(I)     O.
XR(I)     O.
YR(I)     O.
ZRM(I)    O.
12 IF (FU S.LE.C.) GO TO 21
DO 14 I=1,MX
A      = .25*(ZM(I)**2 -YM(I)**2) +FS**2
B      = .5*ZM(I)*YM(I)
S      = SQRT(A**2 +B**2)
T      = O.
IF (S.GT.O.) T = .5*ATAN2(B,A)
IF (B.EC.O.) AND.YM(I).GT.(FS +FS)) T = .5*PI
IF (B.EC.C.) AND.YM(I).LT.-(FS +FS)) T = -.5*PI
S      = SQRT(S)
YM(I)    = .5*YM(I) +S*SIN(T)
ZM(I)    = .5*ZM(I) +S*COS(T)
A      = .25*(ZRM(I)**2 -YRM(I)**2) +FS**2
B      = .5*ZRM(I)*YRM(I)
T      = O.
IF (S.GT.O.) T = .5*ATAN2(B,A)
IF (S.GT.O.) T = .5*ATAN2(B,A)
S      = SQRT(S)
YRM(I)   = .5*YRM(I) +S*SIN(T)
ZRM(I)   = .5*ZRM(I) +S*COS(T)
14 DO 22 I=1,MX
X(I)     = XM(I)
Y(I)     = YM(I)
Z(I)     = ZM(I)
XR(I)    = XRM(I)
YR(I)    = YRM(I)
ZR(I)    = ZRM(I)
XM(I)    = X1*(A0(I)**2 -(B0(J+1) +SO(I,K))**2)
YM(I)    = S2*A0(I)*B0(J+1) +SC(I,K)
ZM(I)    = S1*(A0(I)**2 -(B0(J+1) +SO(I,K))**2)
XR(I)    = SR1*(A0(I)**2 -(B0(J+1) +SO(I,K+1))**2)
YR(I)    = SR2*A0(I)*B0(J+1) +SO(I,K+1)
ZRM(I)   = SR1*(A0(I)**2 -(B0(J+1) +SO(I,K+1))**2)
22 IF (FU S.LE.C.) GO TO 31
DO 24 I=1,MX
A      = .25*(ZM(I)**2 -YM(I)**2) +FS**2

```



```

B S T IF (S.GT.0.) I = .5*ATAN2(B,A) +FS)) T = .5*PI
IF (B.EC.0.) AND .YM(I).LI.-(FS +FS)) T = -.5*PI
IF (B.EC.0.) = SQR(I(S) +S*SIN(I)
S YM(I) = .5*YM(I) +S*CCOS(I)
ZM(I) = .5*ZM(I) +S*CCOS(I)
A B T = .25*(ZRM(I)**2 -YRM(I)**2) +FS**2
I S = .5*ZRM(I)*YRM(I)
T = 0
S I S = SQR(T(A**2 +B**2)
IF (S.GT.0.) T = .5*ATAN2(B,A)
S YRM(I) = SQR(I(S) +S*SIN(I)
ZRM(I) = .5*YRM(I) +S*CCOS(I)
24 DO 32 I=1,NX
31 XX = XR(I+1) +XR(I) +XR(I+1) -XR(I)
1 XY = +X(I+1) -X(I) +XR(I) -XR(I)
1 XZ = +X(I+1) +X(I) -X(I) -XR(I)
1 YX = -X(I+1) +X(I) +XR(I) +XR(I)
1 YY = +Y(I+1) -Y(I) +YRM(I+1) -YRM(I)
1 YZ = +Y(I+1) +Y(I) -Y(I) -YRM(I)
1 ZX = -Y(I+1) +Y(I) +YRM(I+1) +YRM(I)
1 ZY = +Z(I+1) -Z(I) +ZRM(I+1) +ZRM(I)
1 ZZ = +Z(I+1) +Z(I) -Z(I) -ZRM(I)
FX X = YV#ZZ -YZ#ZY
FY X = YZ#ZX -YX#ZZ
FZ X = YX#ZY -YZ#XY
FY Y = ZZ#XX -ZY#XX
FZ Y = ZX#XY -XZ#YY
FX Z = XY#YZ -XX#YX
FZ Z = XX#YY -FY#XY
FM(I) = FX#XX +FZ#XZ
A = 1./FM(I)
GX = G(I+1,J,2) -G(I,J,2) +G(I+1,J+1,2) -G(I,J+1,2)

```



```

GXR      G(I+1,J,3)  -G(I,J,3)  +G(I+1,J+1,3)  -G(I,J+1,3)
GY       G(I+1,J,2)  +G(I,J,2)  -G(I+1,J+1,2)  -G(I,J+1,2)
GXY      G(I+1,J,3)  -G(I,J,3)  -G(I+1,J+1,3)  +G(I,J+1,3)
GX YR    G(I+1,J,3)  -G(I,J,3)  -G(I+1,J+1,3)  +G(I,J+1,3)
GZ       G(I+1,J,3)  -G(I,J,3)  -G(I+1,J+1,3)  +G(I,J+1,3)
1        G(I+1,J,2)  +G(I,J,2)  +G(I+1,J+1,2)  +G(I,J+1,2)
ABM(I)   GXR      -GY
BCM(I)   GXR      -GX
CAM(I)   GXR      -GX
ABCM(I)  GXR      +GY
GX       (FX)X*GX  +FYX*GY  +FZX*GZ)*A  +CA
GY       (FXY)*GX  +FYY*GY  +FZY*GZ)*A  +SA
U        (FXZ)*GX  +FYZ*GY  +FZZ*GZ)*A  +SYAW
V        U*U      +V*V      +W*W
W        AAO      -2*GGM(I)
QQM(I)   ABS(FMACH2*AA)  +FXZ*W
AA        FXX*U    +FXY*V    +FYZ*W
DM(I)    FXX*U    +FXY*V    +FYZ*W
UM(I)    FXX**2   +FXY**2   +FYZ**2
VM(I)    FXX**2   +FXY**2   +FYZ**2
AM(I)    FXX**2   +FXY**2   +FYZ**2
BM(I)    FXX**2   +FXY**2   +FYZ**2
CM(I)    FXX**2   +FXY**2   +FYZ**2
32 DO 34 DM(I)*DM(I)*SQRT(DM(I))
34 DO 36 UM(I)*UM(I)
36 DO 38 DM(I)*VM(I)
38 DO 40 DM(I)*WM(I)
40 DO 42 DM(I)*AM(I)
42 DO 44 DM(I)*EM(I)
44 DO 46 DM(I)*CM(I)
46 DO 48 DM(I)*FM(I)
48 DO 50 (AM(I)+BM(I))*ABM(I)
50 DO 52 (BM(I)+CM(I))*BCM(I)
52 DO 54 (CM(I)+AM(I))*CAM(I)
54 DO 56 (AM(I)+BM(I))*ABCM(I)
56 IF (J.L7.2) GO TO 71
41 DO 42 ABCM(I)
42 IF (J.L7.2) GO TO 71
44 DO 46 QQP(I)  +GCP(I-1)  +QQM(I)  +QQM(I-1)
46 DO 48 FR      +FP(I-1)  +FM(I)  +FM(I-1)
48 DO 50 UR      +UP(I)   +VM(I)  +VM(I-1)
50 DO 52 VR      +VP(I)   +WM(I)  +WM(I-1)
52 DO 54 WR      +WP(I)   +WQ(I)  +WQ(I-1)
54 DO 56 QQ      +WQ(I)   +WQ(I)  +WQ(I-1)
56 DO 58 F       +WQ(I)   +WQ(I)  +WQ(I-1)

```



```

2  B      -ABP(I) +ABP(I-1) +ABM(I) -ABM(I-1)
1  B      WP(I) +WP(I-1) +WM(I) +WM(I-1)
1  B      -BCP(I) -BCP(I-1) +BCM(I) +BCM(I-1)
3  B      -CAP(I) +CAP(I-1) -CAM(I) +CAM(I-1)
RES(I)    +ABCP(I) -ABCP(I-1) -ABCM(I) +ABCM(I-1) +R(I)
RESL(I,J) +AV*(A +B +PF -PB +QP(I) -Q(I)) +RESL(I,J)
AR        = A -B
BR        = AP(I) +AP(I-1) +AM(I) +AM(I-1)
CR        = BP(I) +BP(I-1) +BM(I) +BM(I-1)
A         = CP(I) +CP(I-1) +CM(I) +CM(I-1)
B         = AV*AR
C         = AV*ER
AL(I,J)   = AV*CR
BL(I,J)   = AR
CL(I,J)   = BR
A         = CR
B         = A +B
C         = A +C
TP        = A
TS        = A
S         = A +Q1*(B +C) +Q2*(ABS(FU(I)) +FV(I) +FW(I))
1  F      = (B +Q2*FV(I))*CG(I)
IF (QA(I),LE,I.) GC TG 53
F         = FU(I)
TP        = TP +F
T         = T +3.*(F +FVV(I) +FVW(I)) +F
S         = S +3.*(FVV(I)*CG(I) +FVW(I)*(G(I,J,1) -GL(I,J)))
53  TM     = TP
IF (FU(I).GE.0.) TM = TM +Q2*FU(I) +F +F
IF (FU(I).LT.0.) TP = TP -Q2*FU(I) +F +F
TM        = TM*RESO(I-1)
B         = 1./(T -TM*E(I-1))
D(I)      = B*(RES(I) +S +TM*E(I-1))
E(I)      = B*TP
52  IF (J.LT.J1.OR.K.LT.K1) GO TO 71
I         = I2
CG(I+1)   = 0.
DO 62 M=2,I2
GL(I,J)   = G(I,J,2) +E(I)*CG(I+1)
CG(I)      = D(I) +E(I)*CG(I+1)
GO(I,J,2) = G(I,J,2) +CG(I)
TOTI      = TOTI +1.
AR        = ARS +ABS(RES(I))
IF (ABS(RES(I)).LE.ABS(FRES)) GO TO 63
FRES      = RES(I)
IRES      = I

```


110


```

FM(I)      = FP(I)
VM(I)      = UP(I)
WM(I)      = -VP(I)
AM(I)      = WP(I)
BM(I)      = AP(I)
CM(I)      = BP(I)
ABM(I)     = CP(I)
BCM(I)     = -ABP(I)
CAM(I)     = -BCF(I)
ABCM(I)    = CAP(I)
CONTINLE  = -ABCP(I)
82 DO 92 I=2,NX
  IF (IAES(IV(I,K)).GT.1) GO TO 92
  RESO(I)  = 0.
  A        = 1.
  S        = -AMAXO(0,1ABS(IV(I,K)))
  1 RESL(I,J) = A*(G(I+1,J,2) -G(I,J,2) -G(I,J,2) -G(I-1,J,2) +G(I,J,2) +G(I,J+1,2) +G(I,J+1,2,2)
    AL(I,J) = A
    BL(I,J) = 1.
    CL(I,J) = 0.
92 CONTINLE
GO TO 41
101 S1      = 5*SCAL(K)
    I1      = NX+2 -I2
    I1      = ITE1(K)
    N       = NV
    IF (I.NE.I1.OR.ISYM.EQ.1) GO TO 103
    V       = G(I2,KY,2) -G(I1,KY,2)
    NV      = NV+1
    VORT(NV) = VORT(NV) +P3*(V -VORT(NV))
    N       = NV
    I       = I -1
    103     = 0.
    IF (IV(I,K).NE.1) GC TC 109
    ZZ      = ZO(K) -TYAW*(XO(K) +S1*AO(I)*AO(I))
    105     = ZO(N-1) GO TO 107
    N       = N -1
    GO TO 105
    107     = (ZZ -ZV(N-1))/(ZV(N) -ZV(N-1))
    V       = A*VORT(N) + (1. -A)*VCFI(A-1)
    105     = NX+2 -I
    G(I,KY+1,2) = G(M,KY-1,2) -V
    G(M,KY+1,2) = G(I,KY-1,2) +V
    G(M,KY,2)   = G(I,KY,2) +V
    IF (I.GT.1) GO TO 103
    G(I,KY,2)   = -.5*V

```



```
G(M,KY,2) = .5*V  
G(LX,KY+1,2) = G(LX,KY-1,2)  
RETURN  
END
```



```

Y(I,J)      = YR(I,J)
Z(I,J)      = ZR(I,J)
XR(I,J)      = XRS + S1*(A0(I)**2 - (B0(M) + SC(I,N))**2)
YR(I,J)      = YRS + S2*A0(I)*(B0(M) + SO(I,N))
12 ZR(I,J)   = ZRS
IF (FUS.E.0.) GO TC 21
DO 14 J=1,2
DO 14 I=1,MX
A = .25*(ZR(I,J)**2 - YR(I,J)**2) + FS**2
B = .5*ZR(I,J)*YR(I,J)
S = SQR(A**2 + B**2)
T = 0.
IF (S.GT.0.) T = .5*ATAN2(B,A)
IF (B.EC.0.) AND .YR(I,J).GT.(FS + FS)) T = .5*PI
IF (B.EC.0.) AND .YR(I,J).LT.-(FS + FS)) T = -.5*PI
S = SQR(T)
YR(I,J)      = .5*YR(I,J) + S*SIN(T)
ZR(I,J)      = .5*ZR(I,J) + S*COS(T)
14 ZR(I,J)   = ZR(I,J)
21 IF (N.E.K) GO TC 1
DO 22 I=2,NX
DO 22 J=2,NY
U = 0.
V = 0.
W = 0.
M = 0.
N = 1
XX = X(I+1,1) - X(I,1)
XY = X(I,2) - X(I,1)
XZ = X(I+1,1) - X(I,1)
YX = Y(I+1,1) - Y(I,1)
YZ = Y(I,2) - Y(I,1)
ZX = Z(I+1,1) - Z(I,1)
ZZ = Z(I,2) - Z(I,1)
GX = G(I+1,1) - G(I,1)
GV = G(I,2) - G(I,1)
GZ = G(I+1,1) - G(I,1)
FXX = YZ*ZX - YX*ZZ
FXY = YZ*ZY - YX*ZZ
FYZ = ZY*XX - ZY*XX
FZZ = ZY*XX - ZY*XX
FXZ = XY*YZ - XZ*YX
FYZ = XZ*YX - XZ*YX
FZZ = XX*YX - XX*YX
F = 1. / (FXX*XX + FXY*XY + FZX*XZ)

```



```

25 U = U + (FXX*GX + FYX*GY + FZX*GZ)*F + CA
V = V + (FXY*GX + FYY*GY + FZY*GZ)*F + SA
W = W + (FXZ*GX + FYZ*GY + FZZ*GZ)*F + SYA W
IF (M.EC.2) GO TO 25
M = X(I,1) - X(I-1,1)
XX = Y(I,1) - Y(I-1,1)
YX = Z(I,1) - Z(I-1,1)
ZX = G(I,J,2) - G(I-1,J,2)
GX = GO TO 23
GZ = GO TO 23
IF (N.EC.NMAX) GO TO 27
M = 1
N = X(I+1,1) - X(I,1)
XX = X(I+1,1) - XL(I,1)
XZ = Y(I+1,1) - Y(I,1)
YX = Y(I+1,1) - YL(I,1)
YZ = Z(I+1,1) - Z(I,1)
ZZ = Z(I+1,1) - ZL(I,1)
GX = G(I+1,J,2) - G(I,J,2)
GZ = G(I+1,J,2) - G(I,J,1)
GO TO 23
U = AV*L
V = AV*V
W = AV*h
UU(I) = U
VV(I) = V
WW(I) = W
Q = U*U + V*V + W*h
SV(I) = SQR(T(Q))
SM(I) = AMAX1(.01,1) + Q1*(1. - Q))
CP(I) = FMACH*SV(I)/SQR(T(Q))
XP(I) = T1*(Q*.5 - 1.)
YP(I) = SCAL(KTEL)*X(I,1)
I1 = ITEL(K)
I2 = ITE2(K)
XMAX = SCAL(KTEL)*X(I1,1)
XMIN = SCAL(KTEL)*X(I1,1)
YMAX = SCAL(KTEL)*Y(I1,1)
YMIN = SCAL(KTEL)*Y(I1,1)
DO 22 I=I1,I2
XMAX1(XMAX,XP(I))
XMIN1(XMIN,XP(I))
YMAX1(YMAX,YP(I))
YMIN1(YMIN,YP(I))
22
32 RETURN
END

```



```

C**SUBROUTINE CPLCT*****
SUBROUTINE CPLCT (I3,I4,FMACH,XP,YP,CP,SM,I1,I2,KPLOT)
PLCTS CF AT COMPUTATIONAL MESH PCINTS
COMMON /PCKR/ PTCK
COMMON /PARMT3/ XT3(161), YT3(161), ZT3(161),
1      COMMON /UVW/ UU(161), VV(161), WW(161)
COMMON /PRS/ XOCO(161)
COMMON /SFARE/ LINE(90), DUMY(10)
CIMENSICN KCDE(2), XP(1), YP(1), CP(1), SM(1)
DATA IST/1H*/
DATA I1/1H*/
NOI = C
IMIN = I1 + (I2 - I1)/2
CHC = XF(I1) - XP(IMIN)
2  FOR MAT(40) PLOT OF CP AT COMPUTATIONAL MESH POINTS/
1      COMMON /XCH/ X, Y, 1CH
2      7H XCC, 2X, 5+CP* =, F8.4, 2X, 7HCFGRD =, F10.4
CPC = ((1. + .2*FMACH**2)**3.5 - 1.)/(.7*FMACH**2)
DO 12 I=1,90
12  LINE(I) = KCDE(I)
CPS = ((15. + FMACH**2)/6.)*3.5 - 1.)/(.7*FMACH**2)
IF (KPLOT.EC.O.CR.KPLOT.GT.1) GO TO 15
WRITE (6,2) CPS,CHC
15  CONTINUE
K = 30*(CFO - CPS) + 4.5
IF (KS.GE.1.AND. KS.LE.90) LINE(KS)=IST
DO 22 I=13,14
K = MINC(9C,K)
LINE(K) = XF(I) - XP(IMIN)/CHD
XOCO(I) = XCC
IF (KPLOT.EC.O.CR.KPLOT.GT.1) GO TO 20
WRITE (6,61C) XP(I),YP(I),SM(I),CP(I),XCC,LINE
20  CONTINUE
LINE(K) = KCDE(I)
IF (I.LT.I1.OR.I.GT.I2) GO TO 22
NOI = ACI + 1
XT3(NOI) = XP(I)
YT3(NOI) = YP(I)
ZT3(NOI) = Z
UT3(NOI) = UU(I)
VT3(NOI) = VV(I)
WT3(NOI) = WW(I)
22  IF (K.EC.KS) LINE(KS) = IST
IF (KPLOT.EC.O.CR.KPLOT.GT.1) GO TO 25
CALL INVRT6

```


25 CONTINUE
RETURN
61C FORMAT (2F10.4, F7.4, F8.4, F7.4, 90A1)
END


```

C**SLBROUTINE INVRT6*****
SUBROUTINE INE INVRT6
COMMON /PCKR/ PTCK
COMMON /PARMT3/ XT3(161), YT3(161), ZT3(161),
1 DIMENSION P(161,6), VT3(161), NO1,Z
EQUIVALENCE (XT3(1),P(1,1))
DO 30 J=1,6
DO 10 I=1,NCI
M=NO1-I+1
TEMP(M)=P(I,J)
10 CONTINUE
DO 20 I=1,NCI
P(I,J)=TEMP(I)
20 CONTINUE
30 CONTINUE
1 WRITE (6,100) (I,XT3(I),ZT3(I),YT3(I),UT3(I),
1 WT3(I),VT3(I),I=1,NO1)
RETURN
100 FORMAT (4H0 I ,1X,6HXT3(I),4X,6HZT3(I),4X,6HYT3(I),4X,6HUT3(I),
1 6X,4H I ,1X,6HWT3(I),4X,6HVT3(I),4X,6HUT3(I),4X,6HUT3(I),
2 6X,4H I ,1X,6HWT3(I),4X,6HVT3(I),4X,6HUT3(I),4X,6HUT3(I),
3 6X,4H I ,1X,6HWT3(I),4X,6HVT3(I),4X,6HUT3(I),4X,6HUT3(I),
4 (14,1X,6G10.3,2X,14,1X,6G10.3)
END

```



```

C**SUBROUTINE TCTFOR*****
SUBROUTINE TOTFOR(KTE1,KTE2,CHORD,SCL,SCD,SCM,XO,YPO,ZPO,
1  CL,CD,CMR,CMY)
C  CALCULATES TOTAL FORCE COEFFICIENTS
DIMENSION CHORD(1),SCL(1),SCD(1),SCM(1),XC(1),YPO(1),ZPO(1)
SPAN = ZPO(KTE2) - ZPO(KTE1)
CL = 0.
CD = 0.
CMR = 0.
CMY = 0.
S = 0.
KTE1 = KTE1
KTE2 = KTE2
CHORD(K) = CHORD(K)
SCL(K) = SCL(K)
SCD(K) = SCD(K)
SCM(K) = SCM(K)
XO(K) = XO(K)
YPO(K) = YPO(K)
ZPO(K) = ZPO(K)
1  DO 11
    AZ = .5*(ZPO(K+1) - ZPO(K))
    PL = .5*(ZPO(K+1) + ZPO(K))
    PD = SCL(K+1)*CHORD(K+1)
    PM = SCD(K+1)*CHORD(K+1)
    CL = CHORD(K+1)*(-SCL(K+1)*XO(K+1) + SCD(K+1)*YPO(K+1))
    CDA = DZ*(PL + CL)
    CL = DZ*(PD + QD)
    CL = CL + CLA
    CD = CL + CLA
    CMR = CL + DZ*(PM + QM)
    CMY = CMR + AZ*CLA
    S = CMY + DZ*(CHORD(K+1) + CHORD(K))
    PL = PL
    PD = PD
    PM = PM
    K = K + 1
    IF (K.LT.KTE2) GO TO 11
    CL = CL / S
    CD = CD / S
    CMR = CMR * SPAN / S**2
    CMY = (CMR + CMY) / (S * SPAN)
    CMY = (CMY + CMY) / (S * SPAN)
    RETURN
END

```



```

C**SUBROUTINE REFINE**
C      SUBROUTINE REFINE
C      HALVES PESH
C      COMMON
C      1  SIZE
C      2  G(I1,I1,18,3),SO(I161,35),VORT(115),ZV(115),
C      3  IV(161,35),ITE1(35),ITE2(35),Z0(35),SCAL(35),
C      4  AO(161,18),XO(35),YO(35),Z0(35),KSYN,KFUS,
C      NX,NY,NZ,KTE1,KTE2,ISYN,KSYN,FUS,
C      YAW,CYAW,SYAW,ALPHA,CA,SA,FMACH,N1,N2,N3,I0
C      = NX +1
C      = NY +1
C      = NY +2
C      = NZ +3
C      = NX/2 +1
C      = NY/2 +2
C      = NZ/2 +1
C      = 1
C      IF (KSYN.EQ.0) GC TC 11
C      MZ0 = NZ/2 +3
C      REAC (N1,ERR=401) ((G(I,J,1),I=1,MX0),J=1,MX0)
C      K = 2
C      11 REAC (N1,ERR=401) ((G(I,J,1),I=1,MXC),J=1,MX0)
C      J = NY/2 +1
C      JJ = KY
C      21 I = MX0
C      II = MX
C      31 G(II,JJ,1) = I -1
C      I = I -2
C      IF (I.GT.0) GO TO 31
C      J = J -1
C      JJ = JJ -2
C      IF (J.GT.0) GO TO 21
C      DO 42 J=1,KY,2
C      42 I=2,NX,2
C      G(I,J,1) = .5*(G(I+1,J,1) + G(I-1,J,1))
C      DO 54 I=1,MX,2
C      54 J=2,NY,2
C      G(I,J,1) = .5*(G(I,J+1,1) + G(I,J-1,1))
C      DO 52 G(I,J,1) = 0.
C      52 G(1,NY,1) = 0.
C      G(MX,NY,1) = G(I,J,1),I=1,MX),J=1,MX)
C      WRITE (N2) ((G(I,J,1),I=1,MX),J=1,MX)
C      K = K +1
C      IF (K.LE.MZC) GC TC 11
C      REWIND N1
C      READ (N2,ERR=401) ((G(I,J,1),I=1,MX),J=1,MX)
C      READ (N2,ERR=401) ((G(I,J,3),I=1,MX),J=1,MX)

```



```

WRITE (N1) ((G(I,J,1),I=1,MX),J=1,MY)
K = 1
IF (KSYM.NE.0) K = 2
111 K = K + 1
DO 112 I=1,MY
DO 112 J=1,MX
112 G(I,J,2) = .5*(G(I,J,1) + G(I,J,3))
DO 122 M=2,3
WRITE (N1) ((G(I,J,M),I=1,MX),J=1,MY)
122 CONTINUE
IF (K.EC.MZC) GC TC 201
DO 132 J=1,MY
DO 132 I=1,MX
132 G(I,J,1) = G(I,J,3)
REAC (N2,ERR=401) ((G(I,J,3),I=1,MX),J=1,MY)
GO TO 111
201 REWIND N1
DO 202 M=1,3
DO 202 J=1,MY
DO 202 I=1,MX
REAC (N1,ERR=401) ((G(I,J,M),I=1,MX),J=1,MY)
202 CONTINUE
WRITE (N2) ((G(I,J,1),I=1,MX),J=1,MY)
TYAW = SYAW/CYAW
KTE1 = -1
VORT(NV) = 0.
K = 2
IF (KSYM.NE.0) GO TC 251
211 S1 = .5*SCAL(K)
N = NV
I = MX 0 + 1
IF (K.LT.KTE1.OR.K.GT.KTE2) GO TO 231
11 I = ITE1(K)
12 I = ITE2(K)
DO 212 J=1,I2
DO 212 I=1,I2
G(I,KY+1,2) = NV + 1
G(I,KY,2) + G(I,KY,2) - G(I,KY-1,2)
212 NV = G(I2,KY,2) - G(I1,KY,2)
VORT(NV) = NV
N = NV
I = I1
IF (K.NE.KTE2.OR.YAW.LE.0.) GO TO 231
221 I = I + 1
M = NX + 2 - I
NV = NV + 1
VORT(NV) = G(M,KY,2) - G(I,KY,2)
IF (I.LT.MX0) GC TC 221
231 I = I1 - 1
V = 0.

```



```

IF (IV(I,K).NE.1) GO TO 237
ZZ = ZO(K) -TYAW*(XO(K) +S1*AO(I)*AO(I))
233 IF (ZZ.GE.ZV(N-1)) GO TO 235
N = N -1
GO TO 233
235 A = (ZZ -ZV(N-1))/(ZV(N) -ZV(N-1))
V = A*VCR1(N) +(1. -A)*VCR1(N-1)
237 M = NX +2 -1
G(I,KY+1,2) = G(M,KY-1,2) -V
G(M,KY+1,2) = G(I,KY-1,2) +V
IF (IV(I,K).NE.-1) GO TO 241
G(I,KY,2) = .5*G(I,KY,1) +.25*(G(I,KY,3) +G(M,KY,3))
IF (IV(I,K+1).LT.1)
1G(I,KY,2) = .5*G(I,KY,3) +.25*(G(I,KY,1) +G(M,KY,1))
G(M,KY,2) = .5*G(I,KY,2)
G(I,KY-1,2) = .5*G(I,KY,2) +G(I,KY-2,2)
G(M,KY-1,2) = .5*(G(M,KY,2) +G(M,KY-2,2))
241 IF (I.GT.1) GO TO 231
G(I,KY,2) = -.5*V
G(M,KY,2) = .5*V
251 K = K +1
IF (K.EG.MZ) GO TO 261
DO 252 I=1,MX
DO 252 J=1,MX
G(I,J,1) = G(I,J,2)
G(I,J,2) = G(I,J,3)
252 WRITE (N2) ((G(I,J,1),I=1,MX),J=1,MX)
READ (N1,ERR=401) ((G(I,J,3),I=1,MX),J=1,MX)
GO TO 211
261 VO RT(NV+1) = 0.
DO 262 M=2,3
WRITE (N2) ((G(I,J,M),I=1,MX),J=1,MX)
262 CONTINUE
REWIND N1
REWIND N2
DO 302 K=1,MZ
REAL (N2,ERR=401) ((G(I,J,1),I=1,MX),J=1,MX)
WRITE (N1) ((G(I,J,1),I=1,MX),J=1,MX)
302 CONTINUE
IO = 1
RETURN
401 IO = 0
RETURN
ENC

```



```

C**SUBROUTINE SMGCC**
SUBROUTINE SMOC
SMCGTHS PCTENTIAL
COMMON
1  G(161,18,3),SO(161,35),VORT(115),ZV(115),
2  IV(161,35),ITE1(35),ITE2(35),
3  AO(161,18),XO(35),YC(35),ZO(35),SCAL(35),
4  NX,NY,NZ,KTE1,KTE2,ISYM,KSYM,FUS,
   YAW,CYAW,SYAW,ALPHA,CA,SA,FNACH,N1,N2,N3,IO
   = NX +1
   = NY +1
   = MY +2
   = MZ +3
   = 2
   = NZ
   = 3
   = NZ +2
   = 1./6.
   = 1./6.
   = 1./6.
DO 2 L=1,3
READ (N1,ERR=51) ((G(I,J,L),I=1,MX),J=1,MY)
CONTINUE
WRITE (N2) ((G(I,J,1),I=1,MX),J=1,MY)
K = K1
11 K = K +1
DO 12 J=3,NY
DO 14 I=2,NX
14 G(I,J,1) =
1 2 3
   G(I,J,1) = G(MX,J,2)
   DO 16 I=1,MX
   G(I,1,1) = G(I,1,2)
   G(I,2,1) = G(I,2,2)
   G(I,KY,1) = G(I,KY,2)
   G(I,MY,1) = G(I,MY,2)
16 WRITE (N2) ((G(I,J,1),I=1,MX),J=1,MY)
   IF (K.EC.K2) GO TO 31
   DO 22 I=1,MY
   DO 22 I=1,MX
   G(I,J,1) = G(I,J,2)
22 G(I,J,2) = G(I,J,3)
   READ (N1,ERR=51) ((G(I,J,3),I=1,MX),J=1,MY)
   GO TO 11
31 WRITE (N2) ((G(I,J,3),I=1,MX),J=1,MY)

```



```

REWIND N1
REWIND N2
DO 42 K=1,MZ
  READ (N2,ERR=51) ((G(I,J,1),I=1,MX),J=1,MV)
  WRITE (N1) ((G(I,J,1),I=1,MX),J=1,MV)
42 CONTINUE
   = 1
   = 0
RETURN
51 IO RETURN
END

```



```

C**SUBROUTINE SPLIF*****
SUBROUTINE SPLIF(M,N,S,F,FP,FPP,FPPP,KM,VM,KN,VN,MODE,FQM,IND)
C
C Spline fit - JAMES CN
C INTEGAL PLACED IN FPPP IF MODE GREATER THAN 0
C IND SET TO ZERO IF DATA ILLEGAL
DIMENSION S(1),F(1),FP(1),FPP(1),FPPP(1)
INC = 0
K = IABS(N - M)
IF (K - 1) 81,81,1
1 K = (N - M)/K
I = M
J = M + K
DS = S(J) - S(I)
IF (DS) 11,81,11
11 DF = (F(J) - F(I))/DS
IF (KM - 2) 12,13,14
12 U = .5
13 V = 3.*(DF - VM)/DS
GO TO 25
14 U = 0.
GO TO 25
15 V = -1.*S*VM
GO TO 25
21 I = J
J = J + K
DS = S(J) - S(I)
IF (D*CS) 81,81,23
23 DF = (F(J) - F(I))/DS
B = 1./(DS + DS + U)
U = B*DS
V = B*(6.*DF - V)
FP(I) = U
FPP(I) = V
IF (J - N) 21,21,21
31 IF (KN - 2) 32,33,34
32 V = (6.*VN - V)/U
GO TO 35
33 V = VN
GO TO 35
34 V = (DS*VN + FPP(I))/(1. + FPP(I))
35 B = V
D = DS
41 CS = S(J) - S(I)

```



```

      FPPP(I)  -FF(I)*V
      = (V -U)/DS
      = U
      = (F(J) -F(I))/[S -DS*(V +L +U)/6.
      = U
      = I
      = I -K
      IF (J -M) 41,51,41
51  I FPPP(N)  = N -K
      FPPP(N)  = FPPP(I)
      FPP(N)   = B
      FP(N)    = DF +D*(FPP(I) +B +B)/6.
      IND (MDE) 81,81,61
61  FPPP(J)    = FQM
      V        = FPP(J)
71  I         = J
      J        = J +K
      DS       = S(J) -S(I)
      U        = FPP(J)
      FPPP(J)  = FPPP(I) +.5*DS*(F(I) +F(J) -[S*DS*(U +V)/12.])
      V        = U
      IF (J -N) 71,81,71
      IF (INC.EC.1) GC 71 90
81  WRITET (6,85) INC,MDE,I,J,K,M,S(I),S(J),DS,E
85  FORMAT (6HOCHECK,6I10,4G13.4/)
86  WRITET (6,86) (S(I),F(I),I=M,N)
9C  RETURN
      ENC

```



```

C**SUBROUTINE INTPL**
SUBROUTINE INTP**
INTERPOLATION USING TAYLOR SERIES - JAMESON
ADCS CCFRECTION FOR PIECEWISE CONSTANT FOURTH DERIVATIVE
IF MODE GREATER THAN 0
DIMENSION SI(1),FI(1),S(1),F(1),FPP(1),FPPP(1)
K K = (N -M)/K
I MIN = MI
NIN = NI
D = S(N) -S(M)
IF (D*(SI(NI)) -SI(MI)) 11,13,13
11 MIN = NI
13 KI = ABS(NIN -MIN)
15 KI 21,21,15 = ABS(NIN -MIN)/KI
21 KI = (NIN -KI)
21 II = MIN -KI
C = 0.
IF (MODE) 31,31,23
C I = I +KI
II SS = SI(II)
31 I = I +K
33 IF (I -N) 35,37,35
35 IF (D*(S(I) -SS)) 33,33,37
37 J = I -K
SS FPPP = S(I) -FPPP(I)/(S(J) -S(I))
FF FFF = C*(FPPP(I) +.25*SS*FPPP
FF FFF = FPPP(I) +.5*SS*FF
FF FFF = FPPP(I) +.5*SS*FF
FI(II) = F(I) +SS*FF
IF (II)
41 RETURN
ENC

```



```

C**SUBROUTINE VERTEC*****
1 SUBROUTINE VERTEC(I1,I2,XCCD,CP,NRD,ZPC,FMACH,YA,AL,
   SCL,SCD,SCM,K)
C
C SUBROUTINE FOR VERSATEC PLCTTING OF THE PRESSURE COEFFICIENT
C VS NON-DIMENSIONAL CHORD (X/C) FOR EACH SECTION OF THE FINAL
C MESH
C
   REAL PXC(165),PCP(165),XCLQ(85),XCLP(85),CPLQ(85),CPUP(85),
1   XCCD(161),CP(161),ZPO(35),SCL(35),SCD(35),SCM(35),
2   FMACH,YA,AL
   INTEGER I,J,NUM,NUM1,I1,I2,NRD,K
C
C INITIALIZE ARRAYS AND DATA TO ZERO.
   NUM = 0.0
   NUM1 = 0.0
   DO 10 I=1,165
     PXC(I) = 0.0
     PCP(I) = 0.0
10  CONTINUE
   DO 20 J=1,85
     XCLC(J) = 0.0
     CPLC(J) = 0.0
     XCUP(J) = 0.0
     CPUP(J) = 0.0
20  CONTINUE
C
C READ IN X/C AND CP DATA INTO NEW ARRAY STARTING AT ARRAY
C ELEMENT NUMBER 1
   DO 30 I=1,I2
     PXC(I-I1+1) = XCCD(I)
     PCP(I-I1+1) = CP(I)
30  CONTINUE
   PXC(NRD) = 1.0
C
C PUT THE DATA INTO TWO ARRAYS, ONE FOR THE LOWER SURFACE
C AND ONE FOR THE UPPER SURFACE
   NUM = (NRD-1)/2
   NUM1 = NUM+1
   DO 40 I=1,NLM1
     XCLC(I) = PXC(I)
     CPLC(I) = PCP(I)
40  CONTINUE
   DO 50 J=NUM1,NRD
     XCUP(J-NUM) = PXC(J)
     CPUP(J-NUM) = PCP(J)
50  CONTINUE
C INITIALIZE THE VERSATEC PLCTTER SYSTEM

```



```

C      CALL PLCTS (0.0,0.0,0.0,0)
C
C      SCALE THE DATA TO AN 5.0 X 7.0 INCH SPACE
CALL SCALE (PXC,5.0,NRD,+1)
CALL SCALE (PCP,7.0,NRD,-1)
C
C      DRAW THE X AND Y AXIS
CALL AXIS (1.0,2.0,'X/C',-3,5,0,0,C,PXC(NRD+1),PXC(NRD+2))
CALL AXIS (1.0,2.0,'PRESSURE COEFFICIENT (CF)',25,
>7.0,C,90,C,PCP(NRD+1),PCP(NRD+2))
C      PUT SCALE FACTORS INTO TWO ARRAYS FOR UPPER AND LOWER SURFACE
XCLOC(NUM1+1) = PXC(NRD+1)
XCLOC(NUM1+2) = PXC(NRD+2)
CPLC(NUM1+1) = PCP(NRD+1)
CPLC(NUM1+2) = PCP(NRD+2)
C
XCUP(NUM1+1) = PXC(NRD+1)
XCUP(NUM1+2) = PXC(NRD+2)
CPLUP(NUM1+1) = PCP(NRD+1)
CPLUP(NUM1+2) = PCP(NRD+2)
C
C      PLCT THE DATA PCINTS
CALL NEWPEN (2)
CALL PLCT (1.0,2.0,-3)
CALL LINE (XCLOC,CPLC,NUM1,1,-1,1)
CALL LINE (XCUP,CPLUP,NUM1,1,-1,1)
C
C      PLACE TITLE AT TOP OF PAGE
CALL NEWPEN (3)
CALL SYMBCL (1.25,7.5,0.2,'SECTION CP DATA ',0.0,16)
CALL SYMBCL (1)
CALL SYMBCL (1.25,7.25,0.1,'* = UPPER SURFACE ',0.0,18)
CALL SYMBCL (1.25,7.0,0.1,'+ = LOWER SURFACE ',0.0,18)
C
C      PLACE THE FCCTING INFORMATION ON PLOT
CALL NEWPEN (2)
CALL SYMBCL (0.0,-7.5,0.1,'SPAN STATION = ',0.0,15)
CALL SYMBCL (999.0,0.1,ZPO(K),C.0,+3)
CALL SYMBCL (0.0,-1.0,0.1,'MACF ',0.0,6)
CALL SYMBCL (999.0,0.1,FMACH,0.0,+3)
CALL SYMBCL (2.0,-1.0,0.1,'YAW ',0.0,5)
CALL SYMBCL (999.0,0.1,YA,0.0,+3)
CALL SYMBCL (4.0,-1.0,0.1,'AOA ',0.0,5)
CALL SYMBCL (999.0,0.1,AL,0.0,+3)
CALL SYMBCL (0.0,-1.25,0.1,'CL ',0.0,6)
CALL SYMBCL (999.0,0.1,SCL(K),C.0,+3)
CALL SYMBCL (2.0,-1.25,0.1,'CD ',0.0,5)

```



```

      CALL NUMBER (995., 999., 0.1, SCD(K), 0.0, +5)
      CALL SYMBCL (4.0, -1.25, 0.1, CM, 0.0, +5)
      CALL NUMBER (995., 999., 0.1, SCM(K), 0.0, +5)

C     ENCL PLCTING
      CALL PLCT (0.0, 0.0, +955)
      RETURN
      ENCL

```


APPENDIX F

THIS APPENDIX PRESENTS THE SOURCE CODE FOR THE INTERACTIVE PROGRAM FLO27IN

[illegible]


```

C*****SYMMETRICAL WING SECTION DATA*****
C**DATA SYMFN/59.0/,SYMNUM/59/,
1 1 0000.8500.7500.7000.6500.6000.
2 5000.9500.5000.4000.3000.2500.2000.1500.
3 1250.5000.4500.4000.3500.3000.2500.2000.1500.
4 0050.0025.0000.0025.0050.0100.0150.0200.0250.
5 0350.0500.0750.1000.1250.1500.2000.2500.3000.
6 3500.4000.4500.5000.5500.6000.6500.7000.7500.
7 8000.8500.9000.9500.1.0000.1.0500.1.1000.1.1500.1.2000.
SYMF/ 0025.0075.0130.0180.0240.0290.0340.0375.0415.
1 0450.0475.0505.0525.0550.0575.0600.0625.0650.
2 0480.0447.0398.0330.0265.0200.0140.0080.0020.
3 0090.0065.0000.0065.0030.0000.0000.0000.0000.
4 0230.0265.0330.0398.0447.0500.0550.0600.0650.
5 0550.0555.0550.0525.0505.0475.0450.0425.0400.
6 0375.0340.0290.0240.0180.0130.0075.0025.
7
C*****NACA 24-30-0 SECTION DATA*****
C**DATA N572FN/41.0/,N57NUM/41/,
1 0000.9500.9000.8000.7000.6000.5000.4000.3000.
2 2500.2000.1500.1000.0500.0100.0300.0200.0100.
3 0050.0025.0000.0025.0050.0100.0200.0300.0400.
4 0500.1000.1500.2000.2500.3000.4000.5000.6000.
5 7000.8000.9000.9500.1.0000.1.0500.1.1000.1.1500.1.2000.
N572VF/ 0013.0120.0204.0376.0515.0642.0730.0780.0788.
1 0768.0726.0661.0563.0414.0350.0290.0220.0128.
2 0070.0050.0000.0000.0000.0000.0120.0168.0227.
3 0268.0302.0375.0420.0422.0422.0412.0358.
4 0320.0260.0215.0150.0082.0048.0013.
5
C*****FLAT PLATE DATA*****
C**DATA FFFN/31.0/,FPNUM/31/,
1 0000.5000.0300.0250.0200.0150.0100.0075.0050.
2 0025.0020.0015.0010.0005.0005.0005.0005.0005.
3 0010.0015.0020.0025.0030.0035.0040.0045.0050.
4 0250.0300.0350.0400.0450.0500.0550.0600.0650.
FPVF/ 00003.00003.00003.00003.00003.00003.00003.00003.00003.
1 0000155.0000160.0000165.0000170.0000175.0000180.0000185.0000190.
2 0000045.0000025.0000020.0000015.0000010.0000005.0000000.0000000.
3 0000085.0000080.0000075.0000070.0000065.0000060.0000055.0000050.
4 0000221.0000215.0000210.0000205.0000200.0000195.0000190.0000185.
5 0000221.0000215.0000210.0000205.0000200.0000195.0000190.0000185.
6
C*****F-14 WING SECTION - TYPICAL*****
C**DATA F14FN/47.0/,F14NUM/47/,
1 0000.8500.7500.7000.6500.6000.
2 2571.2000.1429.0857.0571.0286.0171.0114.

```



```

C***      -03500,-03902,-04455,-04782,-04952,-05002,-05067,-050837,
-04412,-03803,-03053,-02187,-01207,-00672,-001057,
C***      *****
DATA N34FN/45.0/N34NUM/45/,
1 2000.0000.9000.8000.7000.6000.5000.4000.3000,
2 2000.1500.1000.0750.0500.0250.0125.0100.0075,
3 0050.0025.0010.0005.0000.0000.0000.0000.0000,
4 0075.0100.0125.0250.0500.0750.1000.1500.2000,
5 3000.4000.5000.6000.7000.8000.9000.9500.1000,
N34 YP/ 00100.00856.01556.02767.03733.04433.04856.05000,
1 04833.04244.03744.03044.02611.02078.01400.00944,
2 00840.00700.00550.00375.00200.0000.0000.0000,
3 00250.00375.00550.00700.00840.00944.01400,
4 002078.002611.003044.003744.004244.04833.05000,
5 04856.04433.03733.02767.01556.00856.00100/
C***      *****
DATA N35FN/45.0/N35NUM/45/,
1 2000.0000.9000.8000.7000.6000.5000.4000.3000,
2 2000.1500.1000.0750.0500.0250.0125.0100.0075,
3 0050.0025.0010.0005.0000.0000.0000.0000.0000,
4 0075.0100.0125.0250.0500.0750.1000.1500.2000,
5 3000.4000.5000.6000.7000.8000.9000.9500.1000,
N35 YP/ 00100.01178.02100.03500.04385.04867.05000.04878,
1 04478.03789.03289.02667.02289.01844.01267.00878,
2 00775.00650.00505.00370.00250.00180.0000.0000,
3 00250.00370.00505.00650.00775.00878.01267,
4 001844.002285.002667.003285.003789.04478.04878,
5 05000.04867.04389.03500.02100.01178.00100/
C***      *****
DATA N64FN/45.0/N64NUM/45/,
1 2000.0000.9000.8000.7000.6000.5000.4000.3000,
2 2000.1500.1000.0750.0500.0250.0125.0100.0075,
3 0050.0025.0010.0005.0000.0000.0000.0000.0000,
4 0075.0100.0125.0250.0500.0750.1000.1500.2000,
5 3000.4000.5000.6000.7000.8000.9000.9500.1000,
N64 YP/ 00100.00856.01556.02767.03733.04433.04856.05000,
1 04856.04411.04056.03533.03178.02722.02044.01511,
2 01395.01210.01000.00730.00480.00350.0000.0000,
3 00480.00730.01000.01210.01395.01511.02044,
4 002722.003178.003533.004056.004411.04856.05000,
5 04856.04433.03733.02767.01556.00856.00100/
C***      *****
DATA N66FN/45.0/N66NUM/45/,
1 2000.0000.9000.8000.7000.6000.5000.4000.3000,

```



```

2000, 1500, 1000, 0750, 0500, 0250, 0125, 0100, 0075,
0050, 0025, 0010, 0005, 0000, 0000, 0000, 0000,
0075, 0100, 0125, 0250, 0500, 0750, 1000, 1500, 2000,
3000, 4000, 5000, 6000, 7000, 8000, 9000, 9500, 1000, 12,
N66 YF/ 00100, 01656, 02833, 04300, 03089, 02656, 02011, 01485,
04578, 04178, 03856, 03400, 03080, 02656, 02011, 01485,
01320, 01170, 00585, 00730, 00985, 01170, 01320, 01485,
00480, 00730, 00985, 01170, 01320, 01485, 02011,
02656, 03085, 03400, 03856, 04178, 04578, 04822,
04956, 05000, 04885, 04300, 02833, 01656, 00100/

```

```

C ***** NACCA 16-005 SECTION DATA *****
DATA N16FN/45 0/N16NUM/45/, 8000, 7000, 6000, 5000, 4000, 3000,
N16 XF/1 0000, 9500, 1000, 0750, 0500, 0250, 0125, 0100, 0075,
0050, 0025, 0010, 0005, 0000, 0000, 0000, 0000, 0000,
0075, 0100, 0125, 0250, 0500, 0750, 1000, 1500, 2000,
3000, 4000, 5000, 6000, 7000, 8000, 9000, 9500, 1000,
N16 YF/ 00090, 01061, 01888, 03145, 03952, 04376, 04500, 04391,
04063, 03498, 03101, 02553, 02274, 01882, 01354, 00969,
00840, 00718, 00595, 00420, 00318, 00215, 0000, 00215,
00300, 00420, 00595, 00718, 00840, 00969, 01354,
01882, 02274, 03101, 03952, 04376, 04500, 04391,
04500, 04376, 03952, 03145, 02274, 01888, 01354, 00969/

```

```

C ***** NACCA 63-010 SECTION DATA *****
DATA N63FN/51 0/N63NUM/51/, 8500, 7500, 7000, 6500, 6000,
N63 XF/1 0000, 9500, 4500, 4000, 3500, 3000, 2500, 2000, 1500,
1000, 0750, 0500, 0250, 0125, 0075, 0050, 0025, 0000,
0075, 0125, 0250, 0500, 0750, 1000, 1500, 2000, 2500,
3000, 3500, 4000, 4500, 5000, 5500, 6000, 6500, 7000,
7500, 8000, 8500, 9000, 9500, 1000, 02166, 02166, 02166,
N63 YF/ 00000, 00214, 00604, 01088, 01618, 02166, 02712, 03234,
03715, 04140, 04496, 04766, 04938, 05000, 04538, 04753,
04445, 03994, 03362, 02950, 02440, 01756, 01275, 01004,
00829, 0000, 0000, 00829, 01000, 01275, 01756, 02440,
02950, 03362, 03715, 04140, 04496, 04766, 04938, 05000,
04938, 04766, 04496, 04140, 03715, 03234, 02712,
02166, 01618, 01088, 0604, 00214, 0000/

```

```

C ***** NACCA 63A010 SECTION DATA *****
DATA N63AFN/51 0/N63AN/51/, 8500, 7500, 7000, 6500, 6000,
N63A XF/1 0000, 9500, 4500, 4000, 3500, 3000, 2500, 2000, 1500,
5500, 5000, 4500, 4000, 3500, 3000, 2500, 2000, 1500,
1000, 0750, 0500, 0250, 0125, 0075, 0050, 0025, 0000,
0075, 0125, 0250, 0500, 0750, 1000, 1500, 2000, 2500,
3000, 3500, 4000, 4500, 5000, 5500, 6000, 6500, 7000,

```



```

6      N63A YP/      .7500 .8000 .8500 .9000 .9500 1.00/ .02545 .03044 .03517,
1      .00021, .00525 .01030 .01535 .02040 .02545 .03044 .03517,
2      .03943, .04311 .04613 .04837 .04968 .04995 .04913 .04714,
3      .04400 .03950 .03324 .02917 .02412 .01737 .01250 .00983,
4      .00815 .0000 .00815 .00583 .01250 .01737 .02412 .03044,
5      .002917, .03324 .03950 .04400 .04714 .04913 .04995,
6      .04968, .04837 .04613 .04311 .03943 .03517 .03044,
7      .02545, .02040 .01535 .01030 .00525, .00021/

C*****
C*****NA CA 64-01C SECTION DATA*****
C*****
DATA N640FN/51.0/, N640N/51/,
1 N640XF/1.0000 .9500 .9000 .8500 .8000 .7500 .7000 .6500 .6000,
2 .5500 .5000 .4500 .4000 .3500 .3000 .2500 .2000 .1500,
3 .1000 .0750 .0500 .0250 .0125 .0075 .0050 .0050,
4 .0075 .0125 .0250 .0500 .1000 .1500 .2000 .2500,
5 .3000 .3500 .4000 .4500 .5000 .5500 .6000 .6500 .7000,
6 .7500 .8000 .8500 .9000 .9500 1.00/,
7 N640 YP/ .0000 .00248 .00671 .01176 .01722 .02281 .02827 .03345,
1 .03820 .04238 .04586 .04843 .04988 .04980 .04864 .04635,
2 .04302 .03842 .03221 .02826 .02343 .01701 .01250 .00985,
3 .00820 .0000 .00820 .00589 .01250 .01701 .02343,
4 .02826, .03221 .03842 .04302 .04635,
5 .04988, .04843 .04586 .04238 .03820 .03345 .02827,
6 .02281, .01722 .01176 .00671 .00248 .0000,
7

C*****
C*****NA CA 64A010 SECTION DATA*****
C*****
DATA N64AFN/51.0/, N64AN/51/,
1 N64AXF/1.0000 .9500 .9000 .8500 .8000 .7500 .7000 .6500 .6000,
2 .5500 .5000 .4500 .4000 .3500 .3000 .2500 .2000 .1500,
3 .1000 .0750 .0500 .0250 .0125 .0075 .0050 .0050,
4 .0075 .0125 .0250 .0500 .1000 .1500 .2000 .2500,
5 .3000 .3500 .4000 .4500 .5000 .5500 .6000 .6500 .7000,
6 .7500 .8000 .8500 .9000 .9500 1.00/,
7 N64A YP/ .00021, .00541 .01062 .01582 .02103 .02623 .03127 .03597,
1 .04021, .04388 .04684 .04854 .04995 .04968 .04837 .04606,
2 .04272 .03813 .03199 .02905 .02327 .01688 .01225 .00969,
3 .00804 .0000 .00804 .00569 .01225 .01688 .02327,
4 .02905, .03199 .03813 .04272 .04606,
5 .04995, .04894 .04684 .04388 .04021 .03597 .03127,
6 .02623, .02103 .01582 .01062 .00541 .00021/

C*****
C*****NA CA 65-010 SECTION DATA*****
C*****
DATA N650FN/51.0/, N650N/51/,
1 N650XF/1.0000 .9500 .9000 .8500 .8000 .7500 .7000 .6500 .6000,
2 .5500 .5000 .4500 .4000 .3500 .3000 .2500 .2000 .1500,
3 .1000 .0750 .0500 .0250 .0125 .0075 .0050 .0050,
4 .0075 .0125 .0250 .0500 .1000 .1500 .2000 .2500,
5 .3000 .3500 .4000 .4500 .5000 .5500 .6000 .6500 .7000,
6 .7500 .8000 .8500 .9000 .9500 1.00/,
7

```



```

6      7500,8000,8500,9000,9500,1000,01987,02584,03156,03682,
1      N650YF/0000,00306,00810,01385,01987,02584,03156,03682,
2      04146,04530,04812,04963,04996,04924,04760,04503,
3      04142,03666,03040,02647,02177,01574,01169,00932,
4      00772,0000,00772,00532,00165,01574,02177,
5      02647,03040,03666,04143,04503,04760,04924,
6      04996,04963,04812,04530,04146,03682,03156,
7      02584,01987,01385,00810,00306,0000/

C*****NACA 65A010 SECTION DATA*****
DATA N65AFN/51.C/,N65AN/51/,
1      N65AXF/1.0000,5500,9000,8500,4000,3500,7000,6500,6000,
2      5500,5000,4500,4000,3500,3000,2500,2000,1500,
3      1000,0750,0250,0125,0075,0050,0050,0050,0050,
4      0075,0125,0250,0500,0750,1000,1500,2000,2500,
5      3000,3500,4000,4500,5000,5500,6000,6500,7000,
6      7500,8000,8500,9000,9500,1000,
7      N65AYF/00021,00604,01188,01771,02352,02912,03432,03859,
1      04304,04632,04863,04983,04995,04912,04742,04483,
2      04127,03658,03040,02650,02182,01623,01183,00928,
3      00765,0000,00765,00528,01183,01623,02182,
4      02650,03040,03658,04127,04483,04742,04912,
5      04995,04983,04863,04632,04304,03899,03432,
6      04912,02352,01771,01188,00604,00021/

C*****NACA 66-010 SECTION DATA*****
DATA N66CFN/51.C/,N66ON/51/,
1      N66OXP/1.0000,9500,9000,8500,4000,3500,7000,6500,6000,
2      5500,5000,4500,4000,3500,3000,2500,2000,1500,
3      1000,0750,0250,0125,0075,0050,0050,0050,0050,
4      0075,0125,0250,0500,0750,1000,1500,2000,2500,
5      3000,3500,4000,4500,5000,5500,6000,6500,7000,
6      7500,8000,8500,9000,9500,1000,
7      N66OYF/0000,00408,01054,01773,02494,03176,03787,04302,
1      04665,04865,04971,05000,04953,04832,04636,04363,
2      04001,03530,02917,02536,02087,01516,01141,00913,
3      00757,0000,02917,03530,04001,04363,04636,04832,
4      04953,05000,04971,04865,04665,04302,03787,
5      03176,02494,01773,01054,00408,0000/

C-----
C FILE DEFINITIONS
C-----
CALL FRICMS ('FILEDEF',5,TERM,,'FLO27',
CALL FRICMS ('FILEDEF',8,DISK,,'
1      CATAIN',A)
C-----

```


C TITLE PAGE AND INSTRUCTIONS

```
CALL FRICMS ('CLRSCRN ')
WRITE (6,410)
WRITE (6,410)
WRITE (6,420)
WRITE (6,430)
WRITE (6,410)
WRITE (6,410)
WRITE (6,440)
WRITE (6,410)
```

C FIRST LINE INPUT DATA--DEFINE COMPUTATIONAL GRID

```
WRITE (6,450)
WRITE (6,460)
READ (5,1000) TITLE
CONTINUE
WRITE (6,470)
READ (5,*) FMESH
WRITE (6,480)
READ (5,*) FNX
WRITE (6,490)
READ (5,*) FNY
CALL FRICMS ('CLRSCRN ')
WRITE (6,500)
READ (5,*) FNZ
WRITE (6,510)
READ (5,*) FPLOT
```

C SUMMARY OF FIRST LINE INPUT DATA

```
CALL FRICMS ('CLRSCRN ')
WRITE (6,520)
READ (5,*) ANS
IF (ANS.GE.2) GO TC 20
WRITE (6,521)
WRITE (6,522) FNX,FNY,FNZ,FMESH,FPLOT
WRITE (6,530)
READ (5,*) ANS
IF (ANS.EQ.1) GO TO 10
20 CONTINUE
```

C SECOND, THIRD AND FORTH LINES INPUT DATA--ITERATION AND CONVERGENCE

```
CTOLERANCE FOR GRID. NUMBER OF LINES EQUAL TO M = FMESH
M = IFI*(FMESH)
CALL FRICMS ('CLRSCRN ')

```



```

WRITE (6,450)
DO 30 I=1,M
  IF (I.EC. 1) WRITE (6,541)
  IF (I.EC. 2) WRITE (6,542)
  IF (I.EC. 3) WRITE (6,543)
  WRITE (6,550)
  REAL (5,*) FIT(I)
  WRITE (6,560)
  REAL (5,*) CCVD(I)
  WRITE (6,570)
  REAL (5,*) P10(I)
  CALL FRICMS ('CLRSCRN ')

```

30 CONTINUE

C-----
C SUMMARY OF SECOND, THIRD AND FORTH LINES INPUT DATA
C-----

```

CALL FRICMS ('CLRSCRN ')
WRITE (6,580)
READ (5,*) ANS
IF (ANS.GE.2) GO TO 40
  WRITE (6,581)
  WRITE (6,582) ( (FIT(I),CCVD(I),P10(I)),I=1,M)
  WRITE (6,590)
  READ (5,*) ANS
  IF (ANS.EQ.1) GO TO 20

```

40 CONTINUE

C-----
C FIFTH LINE INPUT DATA--MACH NO., YAW ANGLE, ADA, SKIN FRICTION DRAG
C-----

```

CALL FRICMS ('CLRSCRN ')
WRITE (6,450)
WRITE (6,600)
READ (5,*) FMACH
WRITE (6,610)
READ (5,*) YA
WRITE (6,620)
READ (5,*) AL
WRITE (6,630)
READ (5,*) CDO

```

C-----
C SUMMARY OF FIFTH LINE INPUT DATA
C-----

```

CALL FRICMS ('CLRSCRN ')
WRITE (6,640)
READ (5,*) ANS
IF (ANS.GE.2) GO TO 50
  WRITE (6,641) FMACH,YA,AL,CDO

```



```

WRITE (6,650)
READ (5,*) ANS
IF (ANS.EQ.1) GO TO 40
50 CONTINUE
C-----
C SIXTH LINE INPUT DATA-----WING PLANFORM SYMMETRY, NUMBER OF SECTIONS,
C SWEEP, DIHEDRAL ANGLE AND FUSELAGE RADIUS
C-----
CALL FRICMS ('CLRSCRN ')
WRITE (6,450)
WRITE (6,660)
READ (5,*) ZSYM
WRITE (6,670)
READ (5,*) FNS
WRITE (6,680)
READ (5,*) SWEEP
WRITE (6,690)
READ (5,*) DIHED
WRITE (6,700)
READ (5,*) FUS
C-----
C SUMMARY OF SIXTH LINE INPUT DATA
C-----
CALL FRICMS ('CLRSCRN ')
WRITE (6,710)
READ (5,*) ANS
IF (ANS.GE.2) GO TO 60
WRITE (6,711) ZSYM,FNS,SWEEP,DIHED,FUS
WRITE (6,720)
READ (5,*) ANS
IF (ANS.EQ.1) GO TO 50
60 CONTINUE
C-----
C WRITE JCL CARDS TO TOP OF FILE ON USER'S "A" DISK
C-----
WRITE (8,1200)
WRITE (8,1210)
C-----
C WRITE FIRST SIX LINES OF DATA TO FILE ON USER'S "A" DISK
C-----
WRITE (8,1010) TITLE
WRITE (8,1020)
WRITE (8,1030) FNX,FNY,FNZ,FMESH,FPLOT
WRITE (8,1040) ((FIT(I),COVO(I),P10(I)),I=1,M)
WRITE (8,1050) FMACH,YA,AL,CDO
WRITE (8,1060)
WRITE (8,1070)

```



```

WRITE (8,1080)
WRITE (8,1090) ZSYM,FNS,SWEEP,CIHEC,FUS
C-----
C SECTION INFLT DATA
C-----
N = IFIX(FNS)
CALL FRTCMS ('CLRSCRN ')
WRITE (6,450)
WRITE (6,730)
WRITE (6,410)
DO 200 I=1,N
  WRITE (6,760) I
  WRITE (6,770)
  REAC (5,*) ZS
  WRITE (6,780)
  REAC (5,*) XL
  WRITE (6,790)
  REAC (5,*) YL
  WRITE (6,800)
  REAC (5,*) CFGRD
  WRITE (6,810)
  REAC (5,*) THICK
  WRITE (6,820)
  REAC (5,*) AT
  CALL FRTCMS ('CLRSCRN ')
  WRITE (6,830)
  REAC (5,*) FSEC
  WRITE (8,1100) ZS,XL,YL,CHORD,THICK,AT,FSEC
  IF (FSEC.EQ.0.0) GO TO 190
  CALL FRTCMS ('CLRSCRN ')
  WRITE (6,450)
  WRITE (6,740)
  WRITE (6,741)
  WRITE (6,750)
  REAC (5,*) ANS
  FLAG = ANS
  IF (FLAG.GT.0) GO TO 70
  WRITE (6,840)
  REAC (5,*) YSYM
  CALL FRTCMS ('CLRSCRN ')
  WRITE (6,850)
  REAC (5,*) FN
C-----
C USER INPUT X AND Y COORDINATES FOR WING SECTION DEFINING GEOMETRY
C-----
NUM = IFIX(FN)
CALL FRTCMS ('CLRSCRN ')

```



```

180 WRITE (6,450) I
    WRITE (6,860) I
    DO 180 J=1,NUM
        WRITE (6,870) J,XP(J),YP(J)
        READ (5,*) XP(J),YP(J)
        CONTINUE
    IF (YSYM .EQ. 0.0) GC TC 185
    N1 = NUM
    J1 = NUM
    DO 183 IA=1,J1
        XP(IA)
        YF(N1-IA) = -YP(IA)
        YF(N1-IA) = -YP(IA)
        CONTINUE
    NUM = N1 + 1 (FN - 1.0)
    FN
    CONTINUE (8,1120)
    WRITE (8,1130) FN
    WRITE (8,1140)
    WRITE (8,1150) ((XP(J),YP(J)),J=1,NUM)
    GO TC 190
    CONTINUE
70

```

```

C-----
C MENU INPUT X AND Y COORDINATES FOR WING SECTION DEFINING GEOMETRY
C-----

```

```

IF (FLAG .EQ. 1) GO TO 81
IF (FLAG .EQ. 2) GO TO 82
IF (FLAG .EQ. 3) GO TO 83
IF (FLAG .EQ. 4) GO TO 84
IF (FLAG .EQ. 5) GO TO 85
IF (FLAG .EQ. 6) GO TO 86
IF (FLAG .EQ. 7) GO TO 87
IF (FLAG .EQ. 8) GO TO 88
IF (FLAG .EQ. 9) GO TO 89
IF (FLAG .EQ. 10) GO TO 90
IF (FLAG .EQ. 11) GC TO 91
IF (FLAG .EQ. 12) GC TO 92
IF (FLAG .EQ. 13) GC TO 93
IF (FLAG .EQ. 14) GC TO 94
IF (FLAG .EQ. 15) GC TO 95
IF (FLAG .EQ. 16) GC TO 96
IF (FLAG .EQ. 17) GC TO 97
IF (FLAG .EQ. 18) GC TO 98
IF (FLAG .EQ. 19) GC TO 99
IF (FLAG .EQ. 20) GO TO 100
CONTINUE (8,1120) FPFN
WRITE (8,1130)

```

81

[illegible]


```

420 FORMAT (/,25X,24HFLO27 DATA INPUT PROGRAM,/,33X,7HAE-4501//)
430 IF A DISK WHICH THIS PROGRAM INTERACTIVELY WRITES A DATA FILE TO YOU
2AL FLOW PROGRAM--FLO27,/)
440 FORMAT (/,8X,57HENTER DATA FOR THE POTENTIAL FLOW PROGRAM IN FREE
1FORMAT (/,8X,52HAFTEER EACH QUESTION THE FORMAT IS GIVEN: (R) -RE
2AL (/,8X,14H1) - INTEGER./,8X,45FEXAMPLE: (R,R) INPUT 2.5,6.789
3OR (1) INPUT 5,/)
450 FORMAT (1X,79H***** FLO27 INPUT PARAMETERS
1*****//)
460 FORMAT (1X,28H=> ENTER THE PROBLEM TITLE:/,5X,20H(64 LETTERS MAX
1IMCM))
470 FORMAT (1X,76H=> ENTER THE NUMBER OF TIMES THE COMPUTATIONAL MESH
1IS REFINED (FMESH): (R),/,1X,22H1.0 = COARSE MESH ONLY,/,1X,27H2.
20 = REFINED TO MEDIUM MESH,/,1X,25H3.0 = REFINED TO FINE MESH)
480 FORMAT (1X,56H=> ENTER THE NUMBER OF COMPUTATIONAL CELLS IN CHCRD
1WISE,/,5X,41HDIRECTION FOR THE INITIAL MESH (FNX): (R),/,5X,47H(MA
2XIMUM NC. = 160/2*N, WHERE N = FMESH - 1.0))
490 FORMAT (1X,63H=> ENTER THE NUMBER OF COMPUTATIONAL CELLS IN NORMA
1L DIRECTION,/,5X,52HFRGM AIRFOIL SURFACE FOR THE INITIAL MESH (FNY
2): (R),/,5X,46H(MAXIMUM NO. = 16/2*N, WHERE N = FMESH - 1.0))
500 FORMAT (1X,55H=> ENTER THE NUMBER OF COMPUTATIONAL CELLS IN SPANW
1ISE,/,5X,41HDIRECTION FOR THE INITIAL MESH (FNZ): (R),/,5X,46H(MA
2XIMUM NC. = 32/2*N, WHERE N = FMESH - 1.0))
510 FORMAT (1X,54H=> ENTER FLAG FOR PRINTER-PLCTING OF CP (FPLOT): (
1R),/,1X,5CHO.0 = PRINTER OUTPUT OF CP WITHOUT PRINTER-PLOT,/,1X
2,47H1.C = PRINTER OUTPUT OF CP WITH CP PRINTER-PLOT,/,1X,57H2.0 =
3PRINTER OUTPUT OF CP AND VERSATEC PLOT OF CP VS X/C,/,7X,34HFOR EA
4CH SECTION OF THE FINAL MESH)
520 FORMAT (1X,33H SUMMARY OF FIRST LINE INPUT DATA?,/,1X,25H=> ENTER
11 = YES, 2 = NO)
521 FORMAT (1X,3HFNZ,7X,3HFNZ,7X,5HFMEH,5X,5HFPLOT)
522 FORMAT (1X,F5.1,5X,F4.1,6X,F3.1,7X,F3.1,/)
530 FORMAT (1X,29HCHANGE FIRST LINE INPUT DATA?,/,1X,25H=> ENTER 1 =
1YES, 2 = NO)
541 FORMAT (26X,28H*** COARSE MESH PARAMETERS***,/)
542 FORMAT (26X,28H*** MEDIUM MESH PARAMETERS***,/)
543 FORMAT (26X,26H*** FINE MESH PARAMETERS***,/)
550 FORMAT (1X,58H=> ENTER MAXIMUM NUMBER OF ITERATIONS FOR MESH (FIT
1): (R),/,5X,41HRECOMMEND: 100 ITERATIONS FOR COARSE MESH,/,17X,29H
220 ITERATIONS FOR MEDIUM MESH,/,17X,27H10 ITERATIONS FOR FINE MESH
3)
560 FORMAT (1X,66H=> ENTER CONVERGENCE TOLERANCE FOR VELOCITY POTENTI
1AL (CCVCL): (R),/,5X,18HRECOMMEND: .000001)
570 FORMAT (1X,62H=> ENTER SUBSONIC PCINI RELAXATION FACTOR FOR MESH
1(P10): (R),/,5X,25HNOTE: VALUE MUST BE < 2.C,/,5X,30HTYPICALLY: 1.
26 FOR COARSE MESH,/,16X,19H1.3 FOR MEDIUM MESH,/,16X,17H1.2 FOR FI
3NE MESH)

```



```

741 7RF CIL (CAMBERED, 1, 1, THICKNESS AT 30% CHORD), /, 6X, 55H8 = NACA 0010
8 (SYMMETRICAL, 10, THICKNESS AT 30% CHORD), /, 6X, 58H9 = NACA 0010-3
94 (SYMMETRICAL, 10, THICKNESS AT 40% CHORD), /, 5X, 59H10 = NACA 0010
>-35 (SYMMETRICAL, 10, THICKNESS AT 50% CHORD), /, 5X, 59H11 = NACA 00
110-64 (SYMMETRICAL, 10, THICKNESS AT 60% CHORD), /, 5X, 59H12 = NACA
20010-66 (SYMMETRICAL, 10, THICKNESS AT 70% CHORD), /, 5X, 58H13 = NACA
3A 16-00C (SYMMETRICAL, 10, THICKNESS AT 80% CHORD), /, 5X, 58H14 = NACA
4A 63-01C (SYMMETRICAL, 10, THICKNESS AT 90% CHORD), /, 5X, 58H15 = NACA
5CA 63A010 (SYMMETRICAL, 10, THICKNESS AT 35% CHORD), /, 5X, 58H16 = N
6ACA 64A010 (SYMMETRICAL, 10, THICKNESS AT 40% CHORD), /, 5X, 58H17 =
7NACA 64A010 (SYMMETRICAL, 10, THICKNESS AT 40% CHORD), /, 5X, 58H18 =
8 NACA 65A010 (SYMMETRICAL, 10, THICKNESS AT 40% CHORD), /, 5X, 58H19 =
1 FCHORD), /, 5X, 58H20 = NACA 66-010 (SYMMETRICAL, 10, THICKNESS AT 45%
2 CHORD), /, 5X, 58H21 = NACA 66-010 (SYMMETRICAL, 10, THICKNESS AT 45%
750 FORMAT (1X, 35H=> ENTER DESIRED NUMBER FROM MENU.)
760 FORMAT (15X, 22H***WING SECTION NUMBER, 12, 1X, 13HPARAMETERS***, /, 5X,
142HNOTE: ALL DIMENSIONS MUST BE IN SAME UNITS.//)
770 FORMAT (1X, 60H=> ENTER THE SPANWISE COORDINATE FOR THIS SECTION (
1ZS): (R))
780 FORMAT (1X, 53H=> ENTER SECTION LEADING EDGE X COORDINATE (XL): (R
1))
790 FORMAT (1X, 53H=> ENTER SECTION LEADING EDGE Y COORDINATE (YL): (R
1))
800 FORMAT (1X, 43H=> ENTER SECTION CHORD LENGTH (CHORD): (R))
810 FORMAT (1X, 55H=> ENTER SECTION THICKNESS SCALING FACTOR (THICK):
1(R))
820 FORMAT (1X, 50H=> ENTER SECTION TWIST ANGLE IN DEGREES (AT): (R))
830 FORMAT (1X, 65H=> ENTER FLAG FOR DEFINING NEW WING SECTION GEOMETR
1Y (FSEC): (R), /, 1X, 40H1.0 = DEFINE A NEW WING SECTION GEOMETRY, /, 1
2X, 67H0.0 = COPY THE WING SECTION GEOMETRY FROM PREVIOUS S
3ECTION, /, 7X, 38HNOTE: FOR FIRST SECTION MUST ENTER 1.0)
840 FORMAT (1X, 44H=> ENTER FLAG FOR INDICATING WHETHER OR NOT, /, 5X, 43H
1THE WING SECTION IS SYMMETRICAL (YSYM): (R), /, 1X, 20H0.0 = ACNSYMMET
2RICAL, /, 1X, 25H1.0 = SYMMETRICAL SECTION, /, 1X, 53HNOTE: IF SYMMETRI
3CAL SECTION UPPER SURFACE.)
850 FORMAT (1X, 58H=> ENTER NUMBER OF WING SECTION DEFINING POINTS (FN
1): (R), /, 1X, 38HNOTE: MAXIMUM NUMBER OF POINTS IS 161.)
860 FORMAT (17X, 22H***WING SECTION NUMBER, 12, 1X, 22HX AND Y COORDINATES
1#*, //)
870 FORMAT (1X, 67H=> ENTER WING SECTION DEFINING POINT X AND Y COORD
1 (XP, YP): (R, R))
880 FORMAT (5X, 64HTHREE ADDITIONAL DATA LINES WILL BE AUTOMATICALLY WR
1ITTEN TO THE, /, 5X, 43HBOTTOM OF YOUR INPUT FILE. THESE LINES ARE: //
2, 5X, 18HEND OF CALCULATIONS, /, 5X, 3HFN, /, 5X, 3H0.0)
890 FORMAT (5X, 70HTHIS COMPLETES THE INPUT DATA. A FILE WITH <FILENAME
1> <FILETYPE> FLG27, /, 5X, 69HDATA IN HAS BEEN WRITTEN TO YOUR "A" DIS

```



```

2K. IF YCL WISH TO MAKE FURTHER,/,5X,62HCHANGES TO YOUR INPUT DATA
3SI MPL Y XEDIT THE CREATED DATA FILE.//,5X,62HTO RUN THE POTENTIAL
4FLCk PFCGRAM (FLO27) USING YOUR DATA FILE,/,5X,61HXEDIT THE FILED
5AND ENTER THE ADDITIONAL CARDS (JOB CARD ETC.),/,5X,60HAS CUTLINED
6 IN THE INSTRUCTIONS, THEN SUBMIT THE FILE TO THE,/,5X,16HBAATCH PR
7OCESOR.//,1X,4HBYE.)
  FORMAT (16(A4))
  FORMAT (1X,16(A4))
  FORMAT (3HFNX,7X,3HFNZ,7X,5HFMESH,5X,5HFPLOT)
  FORMAT (F5.1,5X,F4.1,6X,F3.1,7X,F3.1)
  FORMAT (3HFI,7X,4HCOVC,6X,3HP10)
  FORMAT (F5.1,5X,F7.6,3X,F3.1)
  FORMAT (5HEMAC,5X,2HYA,8X,2HAL,8X,3HCDC)
  FORMAT (F4.2,6X,F3.1,7X,F3.1,7X,F8.6)
  FORMAT (4HZSYM,6X,3HFNS,7X,5HSWEEP,5X,5HDIHED,5X,3HFUS)
  FORMAT (F3.1,7X,F4.1,6X,F6.3,4X,F10.6)
  FORMAT (F3.1,7X,F4.1,6X,F6.3,4X,F10.6)
  FORMAT (2HZS,8X,2HXL,8X,2HYL,8X,5HCHGRD,5X,5HTHICK,5X,
12HAT,8X,4HFSEC)
  FORMAT (6(F8.4,2X),F3.1)
  FORMAT (2HFN)
  FORMAT (F5.1)
  FORMAT (5HXP(1),5X,5HYP(1))
  FORMAT (6F10.7)
  FORMAT (1X,18HEND CF CALCULATION)
  FORMAT (2HFNX)
  FORMAT (F3.1)
  FORMAT (14H// EXEC FLC27)
  FORMAT (17H//GO.SYSIN DD *)
  FORMAT (2H//)
  FORMAT (2H//)
  END

```

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1000
1010
1020
1030
1040
1050
1060
1070
1080
1090
1100
1110
1120
1130
1140
1150
1160
1170
1180
1200
1210
1220
1230

```


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